

# Stormwater Management Design Report

## Bokum Road Business Park

Bokum Road  
Essex, Connecticut

July 1, 2021

Prepared for:

George C. Field Company, Inc.  
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Prepared by:

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# Stormwater Management Design Report

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Essex, Connecticut

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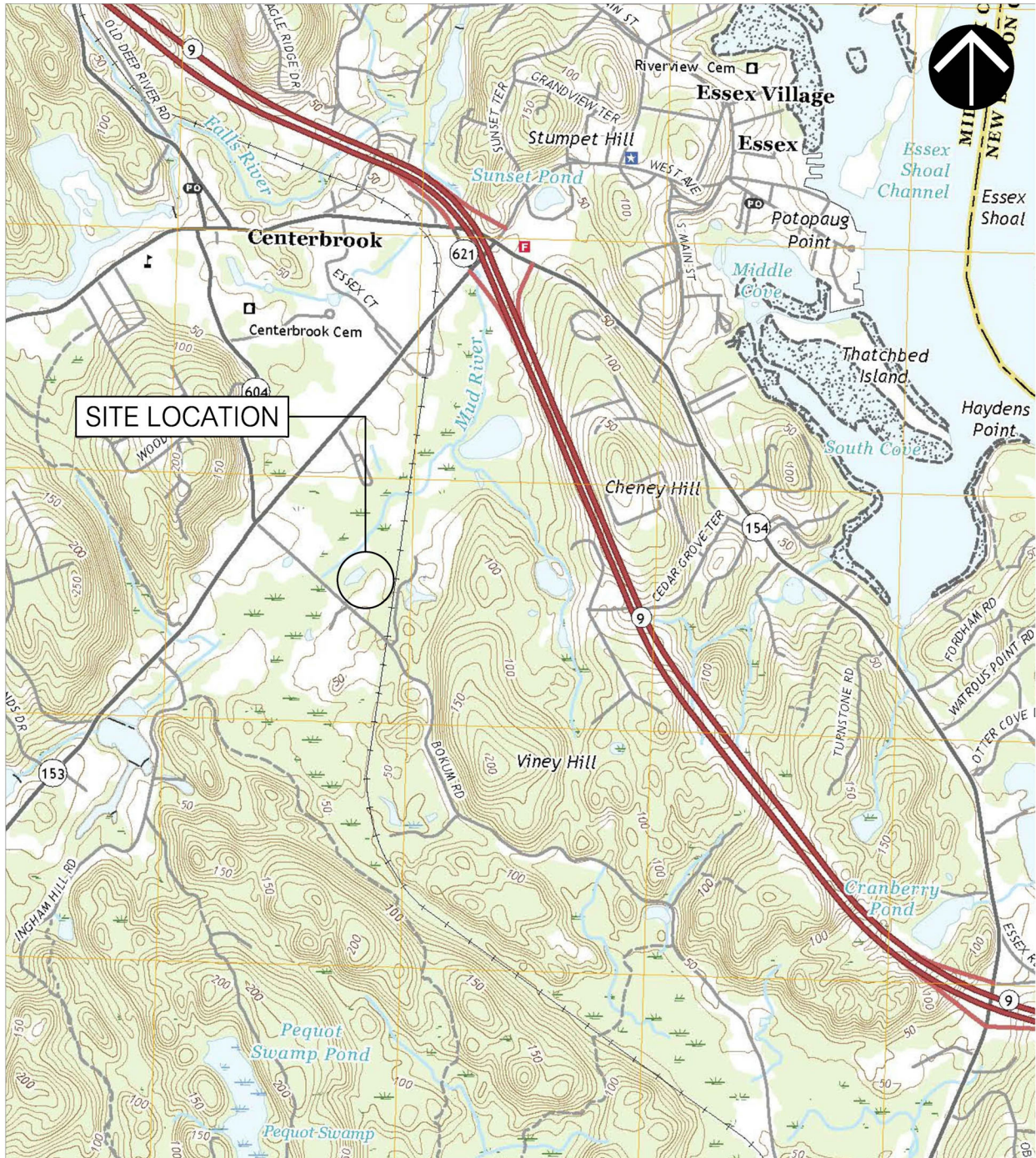
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## 1.0 Introduction

This Stormwater Management Design Report has been prepared on behalf of the George C. Field Company, Inc. who has submitted an application to the Town of Essex Inland Wetlands and Watercourses Commission seeking approval to develop an approximate 8.9 acre land parcel located in the south central portion of the Town of Essex (Figure 1). The parcel is an interior lot located on the north side of Bokum Road approximately 0.35 miles southeast of its intersection with Spencer Plains Road (Conn. Route 153).



**Figure 1.** Project Location  
U.S.G.S. Essex Connecticut Quadrangle

The planned development proposal consists of the construction of a commercial business park. The improvements include a 28,000 square foot building and a 24,800 square foot building and associated access road, driveways, parking area, retaining wall, utility services, on-site wastewater systems, stormwater management facilities, guiderail, signage, and landscaping.

The project site is located within a Limited Industrial (LI) zoning district. The existing land uses adjacent to and in the vicinity of the site are residential and commercial. The project site is undeveloped.

The site is served by the Connecticut Water Company public water system, and public communication, electric, and gas utilities within the Bokum Road right-of-way.

The site is located within the Falls River subregional drainage basin (HUC 4019). The Mud River flows southerly along the site's northerly boundary and to the west of the site and joins Tiffany Brook approximately 0.3 miles to the southwest of the site.

Surface water runoff from the planned development area of the site drains to an inland wetland associated with the Mud River.

The site is located within an un-numbered Special Flood Hazard Area Zone A and Flood Zone X (Figure 2). The planned development portion of the site is partially located within the special flood hazard area zone.

The site is not located within a public water supply watershed area, an aquifer protection area, or an identified Connecticut Department of Energy and Environmental Protection Natural Diversity Database Area.

The Natural Resources Conservation Service Soil Survey of the State of Connecticut indicates that the upland surficial soil types on and in the near vicinity of the planned development portion of the site are classified as Windsor loamy sands, 3-8% slopes (36B).

The approximate area of inland wetland disturbance is 0.02 acres and the disturbed area within the 100-foot inland wetland upland review area is approximately 2.7 acres.

The total area of land disturbance associated with the complete project construction activities is approximately 3.75 acres.

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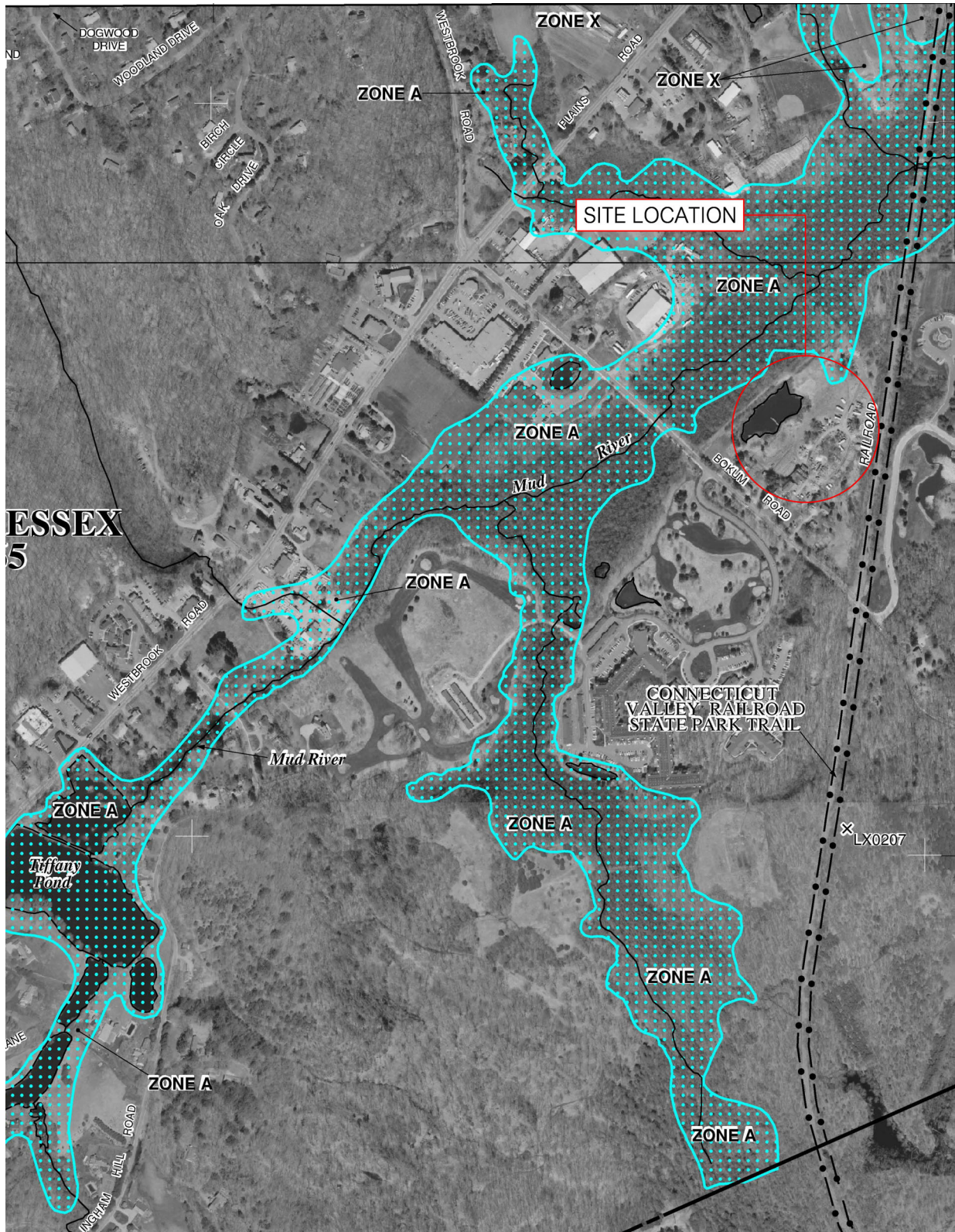


Figure 2. Flood Insurance Rate Map  
 Map No. 00907C0333G

## 2.0 Hydrologic Model Development

The site stormwater management system has been designed in accordance with standard hydrologic and hydraulic engineering practices.

HydroCAD Version 10.10 hydrologic modeling software (HydroCAD Software Solutions, LLC) was used to create the hydrologic models and estimates of peak rates of discharge and volumes of stormwater runoff. The U.S. Department of Agriculture Soil Conservation Service (now Natural Resources Conservation Service) Technical Release 20 Computer Program for Project Formulation Hydrology methodology was used within the HydroCAD software program. TR-20 is a single event, lumped parameter surface water hydrologic model that simulates the precipitation-runoff relationships of a drainage area. The model uses the Soil Conservation Service Curve Number and Unit-Hydrograph methods to represent infiltration losses and to transform excess precipitation into runoff, and the Modified Puls (Storage-Indication) method to perform reservoir routing.

NOAA Precipitation Frequency Atlas 14 for the Northeastern States 24-hour rainfall depths in the project site vicinity shown in Table 1 were accessed from the NOAA precipitation frequency data server and entered into the models.

**Table 1.** 24-Hour Rainfall Depths for the Project Site Vicinity

Recurrence Interval Year	Rainfall Depth Inches
2	3.44
5	4.41
10	5.21
25	6.31
50	7.13
100	8.01

Partial duration series precipitation frequency data was also accessed from the NOAA precipitation frequency data server and entered into the models to create a synthetic rainfall distribution specific to the project site vicinity.

Catchment area boundaries were delineated using the existing conditions mapping for the site. The delineations were checked and adjusted based on a field inspection.

Catchment area composite runoff curve numbers and times of concentration were assumed to be 98 and 0.10 hours respectively using values presented in the National Engineering Handbook, Section 4 - Hydrology (1985).

Antecedent moisture condition II was used to represent the soil moisture condition in the catchment areas prior to the modeled rainfall events.

## 3.0 Stormwater Management System

The site stormwater management system consists of a typical catch basin inlet structure and storm sewer collection and conveyance system that will direct stormwater runoff from the developed sites access road, driveways, parking area, and building roofs to two constructed stormwater wetlands.

The stormwater wetlands have been designed to meet the water quality volume and annual groundwater recharge volume requirements of the Connecticut Department of Energy and Environmental Protection Stormwater Quality Manual for the developed site and to provide a level of attenuation of the rates of peak discharge of stormwater runoff from the developed portion of the site.

The site stormwater collection and conveyance system has been designed in accordance with the procedures outlined in the Connecticut Department of Transportation Drainage Manual. Drainage structure inlets and storm sewers have been designed for peak discharges generated from a 25-year design frequency rainfall event computed using the Rational Method. Outlet protection measures were designed for the 25-year design frequency peak discharge and checked for the 100-year discharge. All times of concentration were assumed to be 5 minutes and all runoff coefficients were assumed to be 0.90.

Stormwater runoff will be directed from the conveyance and collection system to the constructed stormwater wetlands which have been designed to temporarily store runoff and allow it to infiltrate into the underlying natural soils. The water surface elevations (and rates of discharge) for each of the wetlands will be controlled by a V-notch weir principal outlet within a precast concrete outlet control structure. The elevation of the weir crests have been set such that the storage volume below the crests exceeds both the computed water quality volume and annual groundwater recharge volume.

During less frequent, greater depth rainfall events, when the ponded water surface within the wetlands exceeds the elevation of the principal outlet crests, stormwater will be discharged directly to the adjacent natural wetlands.

An overflow inlet grate at the top of each outlet control structure has been set one foot below the top berm elevation of each of the wetlands. The inlet grates have been chosen to have the capacity to pass the 100-year peak discharge with the principal outlet not operating (clogged).

A summary of the rates of peak discharges and the reservoir routing results for the stormwater wetlands are given below.

**Table 2.** Stormwater Wetland 1 - Peak Discharges and Reservoir Routings

	Recurrence Interval					
	2-yr	5-yr	10-yr	25-yr	50-yr	100-yr
Peak Discharge (cfs)	2.9	3.7	4.4	5.3	5.9	6.7
Routed Outflow (cfs)	0.7	1.1	1.4	1.9	2.3	2.7
Peak Stage (ft)	31.5	31.7	31.8	32.0	32.1	32.2

**Table 3.** Stormwater Wetland 2 - Peak Discharges and Reservoir Routings

	Recurrence Interval					
	2-yr	5-yr	10-yr	25-yr	50-yr	100-yr
Peak Discharge (cfs)	4.0	5.2	6.1	7.4	8.4	9.4
Routed Outflow (cfs)	0.9	1.3	1.6	2.1	2.5	2.9
Peak Stage (ft)	22.6	22.7	22.8	22.9	23.0	23.0

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# Summer Hill

Civil Engineers & Land Surveyors, P.C.

BY: MJO      DATE: 7-1-21      SUBJECT: Bokum Road Business Park Essex, Connecticut      SHEET No.: 1 OF 3

CHECKED: LJM      DATE: 7-1-21      Stormwater Management System Design Computations      PROJECT No.: 20-50

1. Water quality volume computed using the CT Stormwater Quality Manual equation

WQV = 1.0 in(R)(A)/12, where:

WQV, Water Quality Volume (Ac-ft)  
 R, Volumetric Runoff Coefficient = 0.05 + 0.009(I)  
 I, Percent impervious cover  
 A, Site area (Ac.)

I = 27.9%  
 R = 0.05 + 0.009(27.9) = 0.30  
 A = 388,259 ft<sup>2</sup> = 8.91 Ac.

WQV = 1 in(R)(A)/12 = (1 in)(0.30)(8.91)/12 = 0.2228 Ac-ft = 9,703 ft<sup>3</sup>

2. Groundwater recharge volume computed using the CT Stormwater Quality Manual equation

GRV = D(A)(I)/12, where:

GRV, Groundwater Recharge Volume (Ac-ft)  
 D, Depth of runoff to be recharged (in)  
 A, Site area (Ac.)  
 I, Net increase in percent of impervious cover

For Hydrologic Soil Group A, D = 0.40 in

A = 388,259 ft<sup>2</sup> = 8.91 Ac.

I (Existing) = 0 ft<sup>2</sup>

I (Proposed) = 108,425 ft<sup>2</sup> / 388,259 ft<sup>2</sup> = 0.279

Net increase = 0.279 - 0 = 0.279

GRV = (0.40 in x 8.91 Ac. x 0.279)/12 = 0.0829 Ac-ft = 3,609 ft<sup>3</sup>

3. Constructed stormwater wetland storage volumes

Stormwater Wetland 1 Stage-Storage

Elevation ft	Area ft <sup>2</sup>	Average Area ft <sup>2</sup>	Incremental Volume ft <sup>3</sup>	Cumulative Volume ft <sup>3</sup>	Cumulative Volume Ac-ft
30.00	3,060	3,060	0	0	0.0000
31.00	3,537	3,299	3,299	3,299	0.0757
32.00	4,038	3,788	3,788	7,086	0.1627
33.00	4,566	4,302	4,302	11,388	0.2614
34.00	5,118	4,842	4,842	16,230	0.3726

Stormwater Wetland 2 Stage-Storage

Elevation ft	Area ft <sup>2</sup>	Average Area ft <sup>2</sup>	Incremental Volume ft <sup>3</sup>	Cumulative Volume ft <sup>3</sup>	Cumulative Volume Ac-ft
22.00	8,590	2,210	0	0	0.0000
23.00	9,430	9,010	9,010	9,010	0.2068
24.00	10,295	9,863	9,863	18,873	0.4333
25.00	11,185	10,740	10,740	29,613	0.6798

## Summer Hill

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BY: MJO      DATE: 7-1-21      SUBJECT: Bokum Road Business Park Essex, Connecticut      SHEET No.: 2 OF 3

CHECKED: LJM      DATE: 7-1-21      Stormwater Management System Design Computations      PROJECT No.: 20-50

#### 4. Outlet control structure inlet grate capacity computations

Grate inlet capacity using ConnDOT Drainage Manual equations:

Capacity of grate inlets operating as a weir ( $0 \text{ ft} \leq d \leq 0.4 \text{ ft}$ ):

$Q = CPd^{1.5}/CFS$ , where:

Q, Discharge (cfs)

C, Weir Discharge Coefficient = 3.0

P, Grate perimeter (ft)

d, Depth over grate (ft)

CFS, Factor of safety for clogging = 1.0 - 2.0

Capacity of grate inlets operating as an orifice ( $d \geq 1.4 \text{ ft}$ ):

$Q = CA(2gd)^{0.5}/CFS$ , where:

Q, Discharge (cfs)

C, Orifice Discharge Coefficient = 0.67

A, Grate clear opening area (ft<sup>2</sup>)

g, Gravitational constant = 32.2 (ft/s<sup>2</sup>)

d, Depth over grate (ft)

CFS, Factor of safety for clogging = 1.0 - 2.0

Check grate inlet capacities for maximum 100-year inflow peak discharge = 9.4 cfs and a water surface elevation depth of 1.0 feet (equal to the top of berm elevations):

Grate perimeter (P) = (4 + 4 + 4 + 4)ft = 16.0 ft

Grate clear open area (A) (ignore openings at grate perimeter):

4 rows x 10 rows = 40 openings

40 x (0.3125 ft x 0.6458 ft) = 8.1 ft<sup>2</sup>

$Q_w = 3.0(16.0)(1.00)^{1.5}/2.0 = 24.0 \text{ cfs}$

$Q_o = 0.67(8.1)(2(32.2)(1.00))^{0.5}/2.0 = 21.8 \text{ cfs}$

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## Summer Hill

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BY: MJO      DATE: 7-1-21      SUBJECT: Bokum Road Business Park Essex, Connecticut      SHEET No.: 3 OF 3

CHECKED: LJM      DATE: 7-1-21      Stormwater Management System Design Computations      PROJECT No.: 20-50

### 5. Outlet Protection Computations

Riprap apron dimensions based on ConnDOT Drainage Manual design procedure:

Using critical depth (dc) as tailwater depth (TW), dc for maximum design discharge ( $Q_{100}$ ) =  $9.4 \text{ ft}^3/\text{s} = 1.1 \text{ ft}$

$$1.1 \text{ ft} > 0.5R_p = 0.5(1.5) = 0.75 \text{ ft}$$

Type B Riprap Apron (maximum tailwater condition) dimensions:

$$L_a = (3.0(Q - 5)/S_p^{1.5}) + 10$$

$$W_1 = 3 S_p \text{ (min.)}$$

$$W_2 = 3 S_p + 0.4 L_a$$

Q    Design Discharge ( $\text{ft}^3/\text{s}$ )

$S_p$     Pipe Span (ft)

$R_p$     Pipe Rise (ft)

$L_a$     Length of Apron (ft)

$W_1$     Width of Apron at Pipe Outlet (ft)

$W_2$     Width of Apron at Apron Outlet (ft)

$$Q_{100} = 9.4 \text{ ft}^3/\text{s}$$

$$S_p = 1.5 \text{ ft}$$

$$R_p = 1.5 \text{ ft}$$

$$L_a = 3.0(9.4 - 5)/1.5^{1.5} + 10 = 17.2 \text{ ft} - \text{Use } 18 \text{ ft}$$

$$W_1 = 3(1.5) = 4.5 \text{ ft} - \text{Use } 5 \text{ ft}$$

$$W_2 = 3(1.5) + 0.4(18.0) = 11.7 \text{ ft} - \text{Use } 12 \text{ ft}$$

Use modified riprap ( $D_{50} = 0.42 \text{ ft}$ )

Depth (d) = 1.0 ft

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Appendix B  
Hydrologic Model Input Data and Results

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**20-50 SWL1**

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**Rainfall Events Listing (selected events)**

Event#	Event Name	Storm Type	Curve	Mode	Duration (hours)	B/B	Depth (inches)	AMC
1	2-yr	CT-Essex 24-hr S1	2-yr	Default	24.00	1	3.44	2
2	5-yr	CT-Essex 24-hr S1	5-yr	Default	24.00	1	4.41	2
3	10-yr	CT-Essex 24-hr S1	10-yr	Default	24.00	1	5.21	2
4	25-yr	CT-Essex 24-hr S1	25-yr	Default	24.00	1	6.31	2
5	50-yr	CT-Essex 24-hr S1	50-yr	Default	24.00	1	7.13	2
6	100-yr	CT-Essex 24-hr S1	100-yr	Default	24.00	1	8.01	2

**20-50 SWL1**

*CT-Essex 24-hr S1 2-yr Rainfall=3.44"*

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Time span=0.00-24.10 hrs, dt=0.05 hrs, 483 points  
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN  
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

**Subcatchment20: DA 1**

Runoff Area=34,790 sf 100.00% Impervious Runoff Depth>3.21"  
Tc=6.0 min CN=98 Runoff=2.89 cfs 0.213 af

**Pond 25: SWL 1**

Peak Elev=31.53' Storage=5,306 cf Inflow=2.89 cfs 0.213 af  
Outflow=0.75 cfs 0.188 af

**Total Runoff Area = 0.799 ac Runoff Volume = 0.213 af Average Runoff Depth = 3.21"**  
**0.00% Pervious = 0.000 ac 100.00% Impervious = 0.799 ac**

**20-50 SWL1**

CT-Essex 24-hr S1 2-yr Rainfall=3.44"

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**Summary for Subcatchment 20: DA 1**

Runoff = 2.89 cfs @ 12.04 hrs, Volume= 0.213 af, Depth> 3.21"  
 Routed to Pond 25 : SWL 1

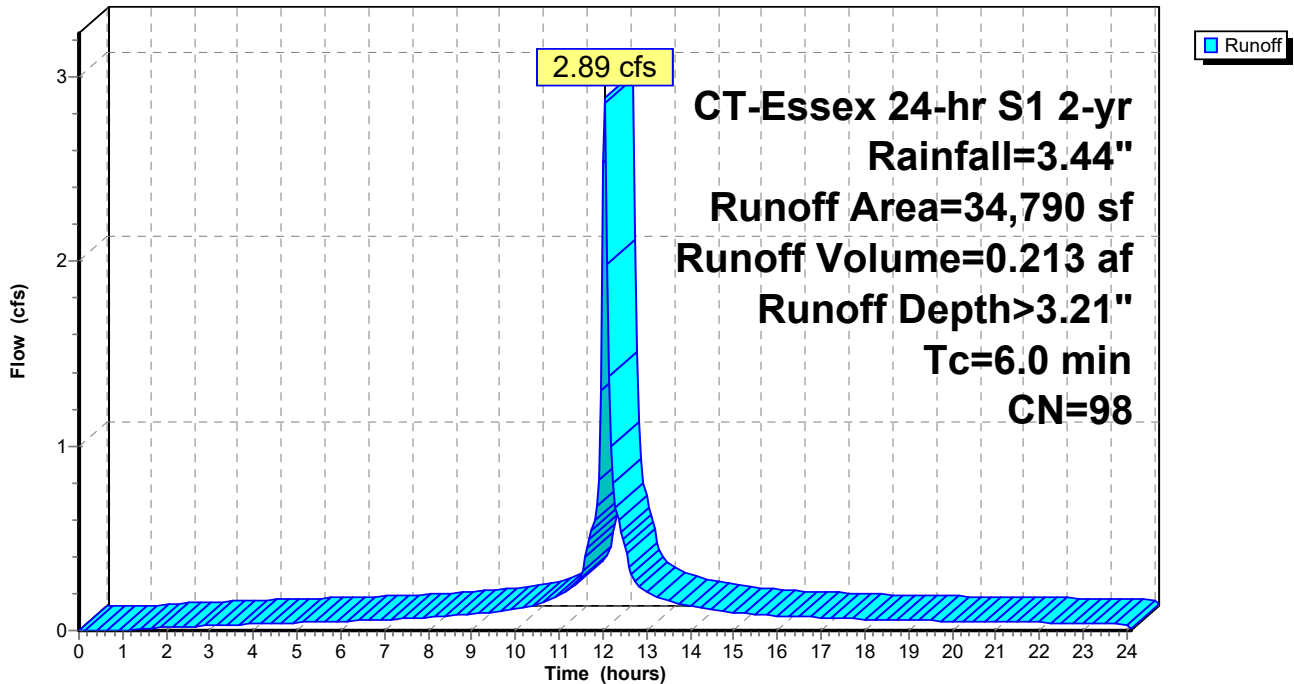
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.10 hrs, dt= 0.05 hrs  
 CT-Essex 24-hr S1 2-yr Rainfall=3.44"

Area (sf)	CN	Description
* 34,790	98	
34,790		100.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Subcatchment 20: DA 1**

Hydrograph



**20-50 SWL1**

CT-Essex 24-hr S1 2-yr Rainfall=3.44"

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**Summary for Pond 25: SWL 1**

Inflow Area = 0.799 ac, 100.00% Impervious, Inflow Depth > 3.21" for 2-yr event  
 Inflow = 2.89 cfs @ 12.04 hrs, Volume= 0.213 af  
 Outflow = 0.75 cfs @ 12.27 hrs, Volume= 0.188 af, Atten= 74%, Lag= 13.9 min  
 Primary = 0.75 cfs @ 12.27 hrs, Volume= 0.188 af

Routing by Stor-Ind method, Time Span= 0.00-24.10 hrs, dt= 0.05 hrs  
 Starting Elev= 30.50' Storage= 1,650 cf  
 Peak Elev= 31.53' @ 12.27 hrs Storage= 5,306 cf (3,656 cf above start)

Plug-Flow detention time= 286.0 min calculated for 0.150 af (70% of inflow)  
 Center-of-Mass det. time= 112.7 min ( 869.8 - 757.2 )

Volume	Invert	Avail.Storage	Storage Description
#1	30.00'	16,231 cf	<b>Custom Stage Data</b> Listed below

Elevation (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
30.00	0	0
31.00	3,299	3,299
32.00	3,788	7,087
33.00	4,302	11,389
34.00	4,842	16,231

Device	Routing	Invert	Outlet Devices
#1	Primary	30.00'	<b>15.0" Round Culvert</b> L= 14.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 30.00' / 29.93' S= 0.0050 ' / ' Cc= 0.900 n= 0.012, Flow Area= 1.23 sf
#2	Device 1	30.50'	<b>30.0 deg x 2.33' rise Sharp-Crested Vee/Trap Weir</b> Cv= 2.61 (C= 3.26)

**Primary OutFlow** Max=0.75 cfs @ 12.27 hrs HW=31.53' (Free Discharge)

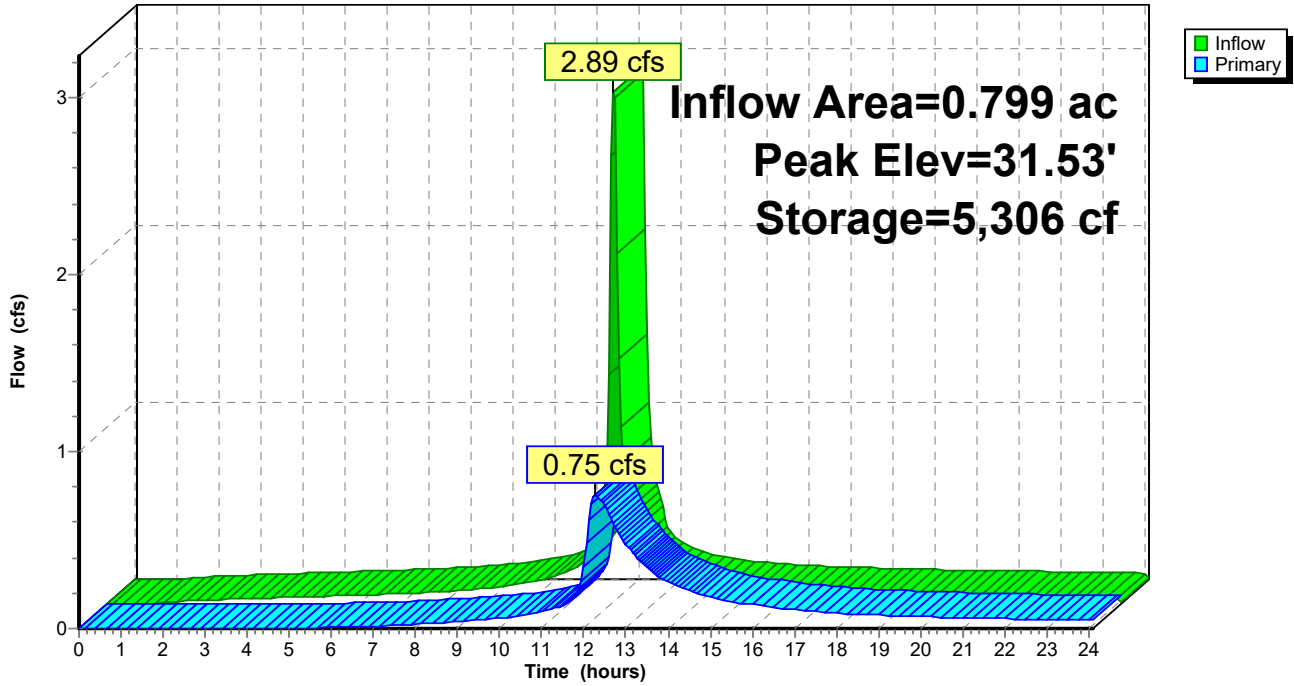
↑1=Culvert (Passes 0.75 cfs of 4.85 cfs potential flow)

↑2=Sharp-Crested Vee/Trap Weir (Weir Controls 0.75 cfs @ 2.65 fps)



Pond 25: SWL 1

Hydrograph



**20-50 SWL1**

*CT-Essex 24-hr S1 5-yr Rainfall=4.41"*

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Time span=0.00-24.10 hrs, dt=0.05 hrs, 483 points  
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN  
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

**Subcatchment20: DA 1**

Runoff Area=34,790 sf 100.00% Impervious Runoff Depth>4.17"  
Tc=6.0 min CN=98 Runoff=3.70 cfs 0.278 af

**Pond 25: SWL 1**

Peak Elev=31.71' Storage=5,970 cf Inflow=3.70 cfs 0.278 af  
Outflow=1.12 cfs 0.250 af

**Total Runoff Area = 0.799 ac Runoff Volume = 0.278 af Average Runoff Depth = 4.17"**  
**0.00% Pervious = 0.000 ac 100.00% Impervious = 0.799 ac**

**20-50 SWL1**

CT-Essex 24-hr S1 5-yr Rainfall=4.41"

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**Summary for Subcatchment 20: DA 1**

Runoff = 3.70 cfs @ 12.04 hrs, Volume= 0.278 af, Depth> 4.17"  
Routed to Pond 25 : SWL 1

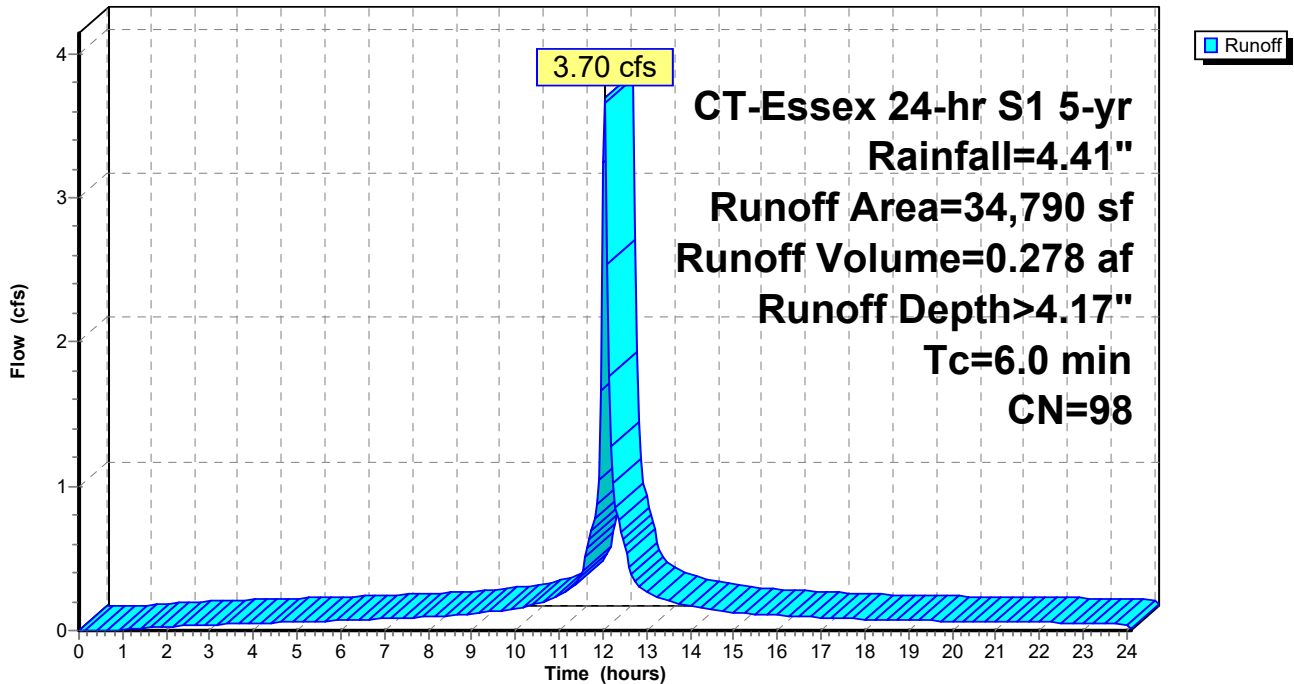
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.10 hrs, dt= 0.05 hrs  
CT-Essex 24-hr S1 5-yr Rainfall=4.41"

Area (sf)	CN	Description
* 34,790	98	
34,790		100.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Subcatchment 20: DA 1**

Hydrograph



**Summary for Pond 25: SWL 1**

Inflow Area = 0.799 ac, 100.00% Impervious, Inflow Depth > 4.17" for 5-yr event  
 Inflow = 3.70 cfs @ 12.04 hrs, Volume= 0.278 af  
 Outflow = 1.12 cfs @ 12.23 hrs, Volume= 0.250 af, Atten= 70%, Lag= 11.8 min  
 Primary = 1.12 cfs @ 12.23 hrs, Volume= 0.250 af

Routing by Stor-Ind method, Time Span= 0.00-24.10 hrs, dt= 0.05 hrs  
 Starting Elev= 30.50' Storage= 1,650 cf  
 Peak Elev= 31.71' @ 12.23 hrs Storage= 5,970 cf (4,321 cf above start)

Plug-Flow detention time= 252.5 min calculated for 0.212 af (76% of inflow)  
 Center-of-Mass det. time= 100.4 min ( 852.1 - 751.7 )

Volume	Invert	Avail.Storage	Storage Description
#1	30.00'	16,231 cf	<b>Custom Stage Data</b> Listed below

Elevation (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
30.00	0	0
31.00	3,299	3,299
32.00	3,788	7,087
33.00	4,302	11,389
34.00	4,842	16,231

Device	Routing	Invert	Outlet Devices
#1	Primary	30.00'	<b>15.0" Round Culvert</b> L= 14.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 30.00' / 29.93' S= 0.0050 ' / ' Cc= 0.900 n= 0.012, Flow Area= 1.23 sf
#2	Device 1	30.50'	<b>30.0 deg x 2.33' rise Sharp-Crested Vee/Trap Weir</b> Cv= 2.61 (C= 3.26)

**Primary OutFlow** Max=1.11 cfs @ 12.23 hrs HW=31.70' (Free Discharge)

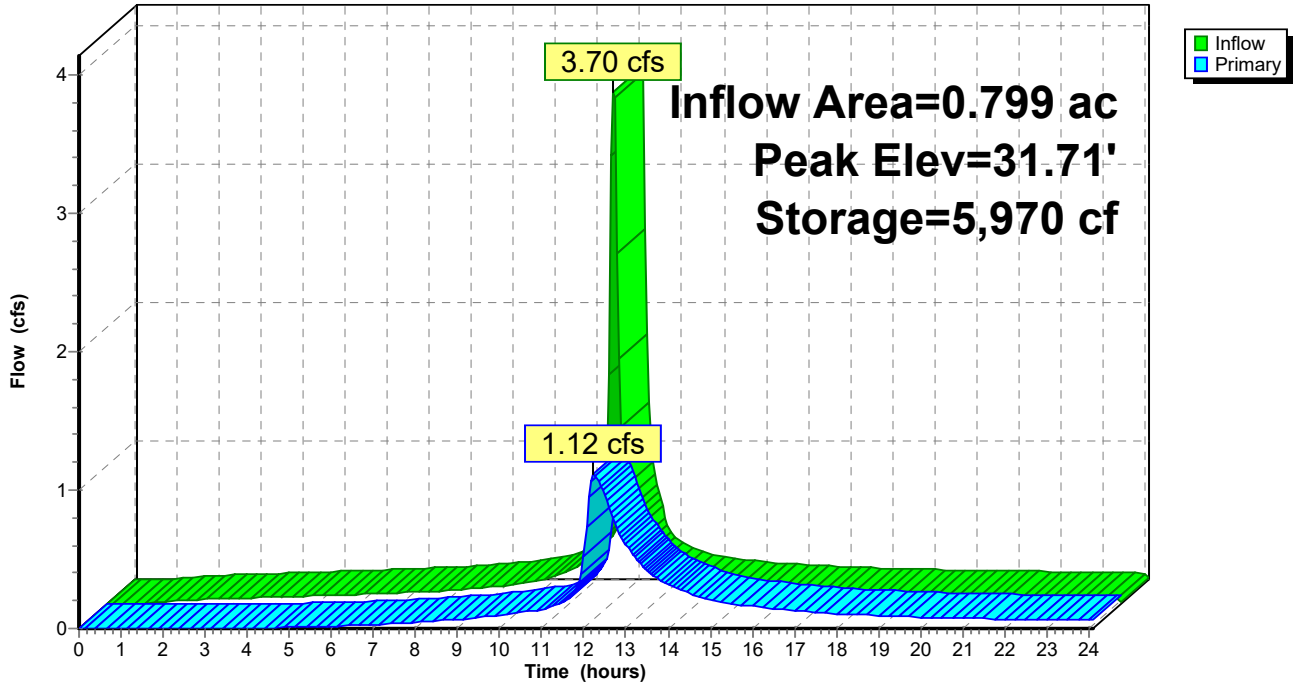
↑1=Culvert (Passes 1.11 cfs of 5.35 cfs potential flow)

↑2=Sharp-Crested Vee/Trap Weir (Weir Controls 1.11 cfs @ 2.86 fps)



Pond 25: SWL 1

Hydrograph



**20-50 SWL1**

*CT-Essex 24-hr S1 10-yr Rainfall=5.21"*

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Time span=0.00-24.10 hrs, dt=0.05 hrs, 483 points  
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN  
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

**Subcatchment20: DA 1**

Runoff Area=34,790 sf 100.00% Impervious Runoff Depth>4.97"  
Tc=6.0 min CN=98 Runoff=4.37 cfs 0.331 af

**Pond 25: SWL 1**

Peak Elev=31.84' Storage=6,469 cf Inflow=4.37 cfs 0.331 af  
Outflow=1.45 cfs 0.301 af

**Total Runoff Area = 0.799 ac Runoff Volume = 0.331 af Average Runoff Depth = 4.97"**  
**0.00% Pervious = 0.000 ac 100.00% Impervious = 0.799 ac**

**20-50 SWL1**

CT-Essex 24-hr S1 10-yr Rainfall=5.21"

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**Summary for Subcatchment 20: DA 1**

Runoff = 4.37 cfs @ 12.04 hrs, Volume= 0.331 af, Depth> 4.97"  
Routed to Pond 25 : SWL 1

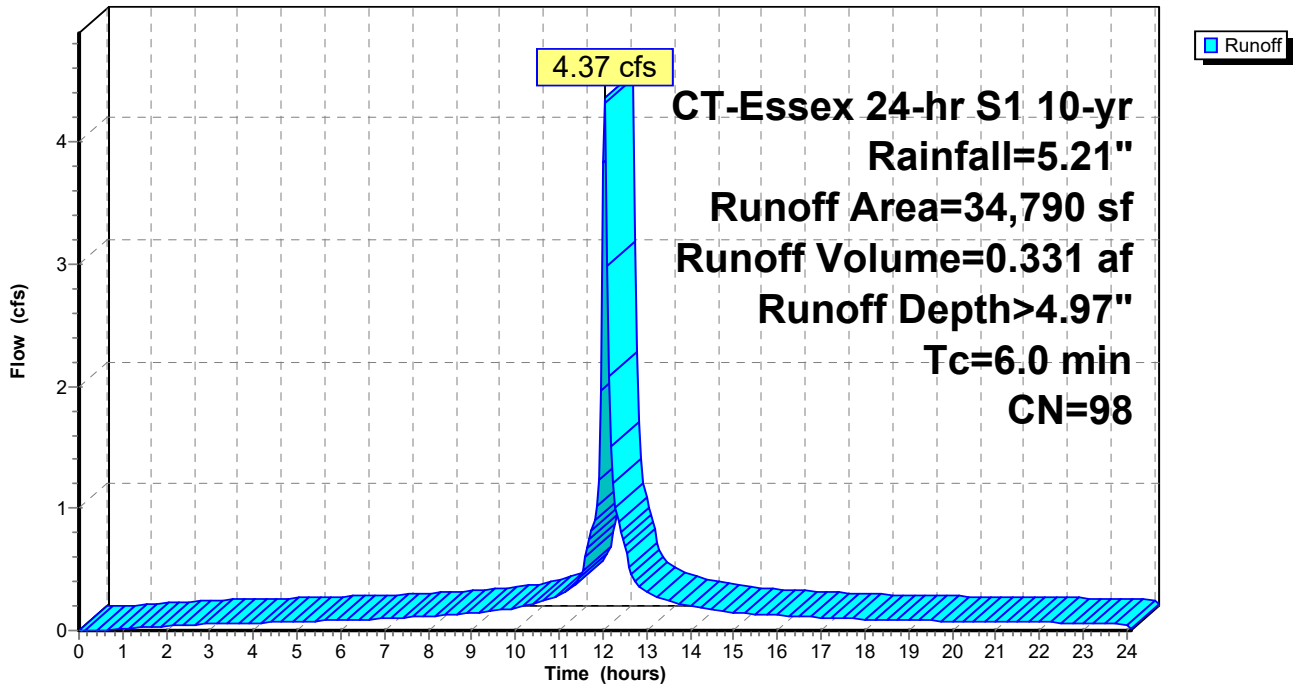
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.10 hrs, dt= 0.05 hrs  
CT-Essex 24-hr S1 10-yr Rainfall=5.21"

Area (sf)	CN	Description
* 34,790	98	
34,790		100.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Subcatchment 20: DA 1**

Hydrograph



**Summary for Pond 25: SWL 1**

Inflow Area = 0.799 ac, 100.00% Impervious, Inflow Depth > 4.97" for 10-yr event  
 Inflow = 4.37 cfs @ 12.04 hrs, Volume= 0.331 af  
 Outflow = 1.45 cfs @ 12.22 hrs, Volume= 0.301 af, Atten= 67%, Lag= 10.7 min  
 Primary = 1.45 cfs @ 12.22 hrs, Volume= 0.301 af

Routing by Stor-Ind method, Time Span= 0.00-24.10 hrs, dt= 0.05 hrs  
 Starting Elev= 30.50' Storage= 1,650 cf  
 Peak Elev= 31.84' @ 12.22 hrs Storage= 6,469 cf (4,820 cf above start)

Plug-Flow detention time= 231.9 min calculated for 0.263 af (79% of inflow)  
 Center-of-Mass det. time= 92.8 min ( 841.2 - 748.4 )

Volume	Invert	Avail.Storage	Storage Description
#1	30.00'	16,231 cf	<b>Custom Stage Data</b> Listed below

Elevation (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
30.00	0	0
31.00	3,299	3,299
32.00	3,788	7,087
33.00	4,302	11,389
34.00	4,842	16,231

Device	Routing	Invert	Outlet Devices
#1	Primary	30.00'	<b>15.0" Round Culvert</b> L= 14.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 30.00' / 29.93' S= 0.0050 ' / ' Cc= 0.900 n= 0.012, Flow Area= 1.23 sf
#2	Device 1	30.50'	<b>30.0 deg x 2.33' rise Sharp-Crested Vee/Trap Weir</b> Cv= 2.61 (C= 3.26)

**Primary OutFlow** Max=1.44 cfs @ 12.22 hrs HW=31.83' (Free Discharge)

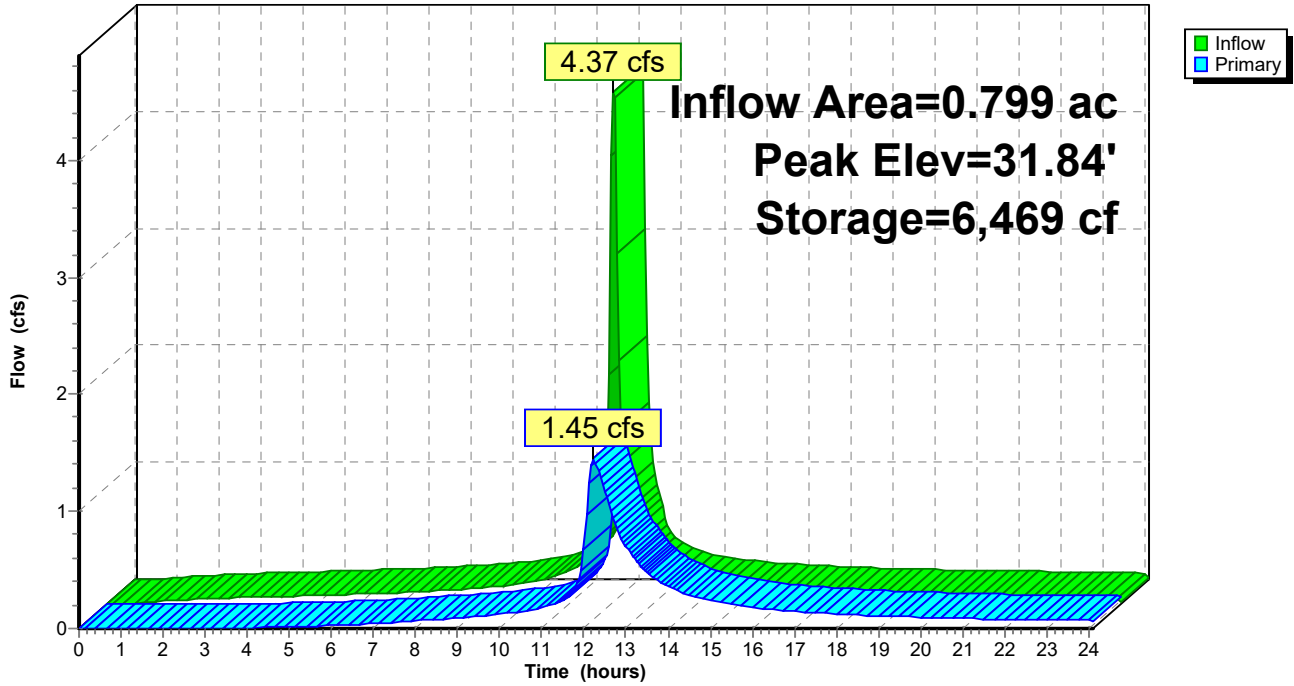
↑ **1=Culvert** (Passes 1.44 cfs of 5.97 cfs potential flow)

↑ **2=Sharp-Crested Vee/Trap Weir** (Weir Controls 1.44 cfs @ 3.02 fps)



Pond 25: SWL 1

Hydrograph



**20-50 SWL1**

*CT-Essex 24-hr S1 25-yr Rainfall=6.31"*

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Time span=0.00-24.10 hrs, dt=0.05 hrs, 483 points  
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN  
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

**Subcatchment20: DA 1**

Runoff Area=34,790 sf 100.00% Impervious Runoff Depth>6.07"  
Tc=6.0 min CN=98 Runoff=5.29 cfs 0.404 af

**Pond 25: SWL 1**

Peak Elev=32.00' Storage=7,096 cf Inflow=5.29 cfs 0.404 af  
Outflow=1.93 cfs 0.372 af

**Total Runoff Area = 0.799 ac Runoff Volume = 0.404 af Average Runoff Depth = 6.07"**  
**0.00% Pervious = 0.000 ac 100.00% Impervious = 0.799 ac**

**20-50 SWL1**

CT-Essex 24-hr S1 25-yr Rainfall=6.31"

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**Summary for Subcatchment 20: DA 1**

Runoff = 5.29 cfs @ 12.04 hrs, Volume= 0.404 af, Depth> 6.07"  
 Routed to Pond 25 : SWL 1

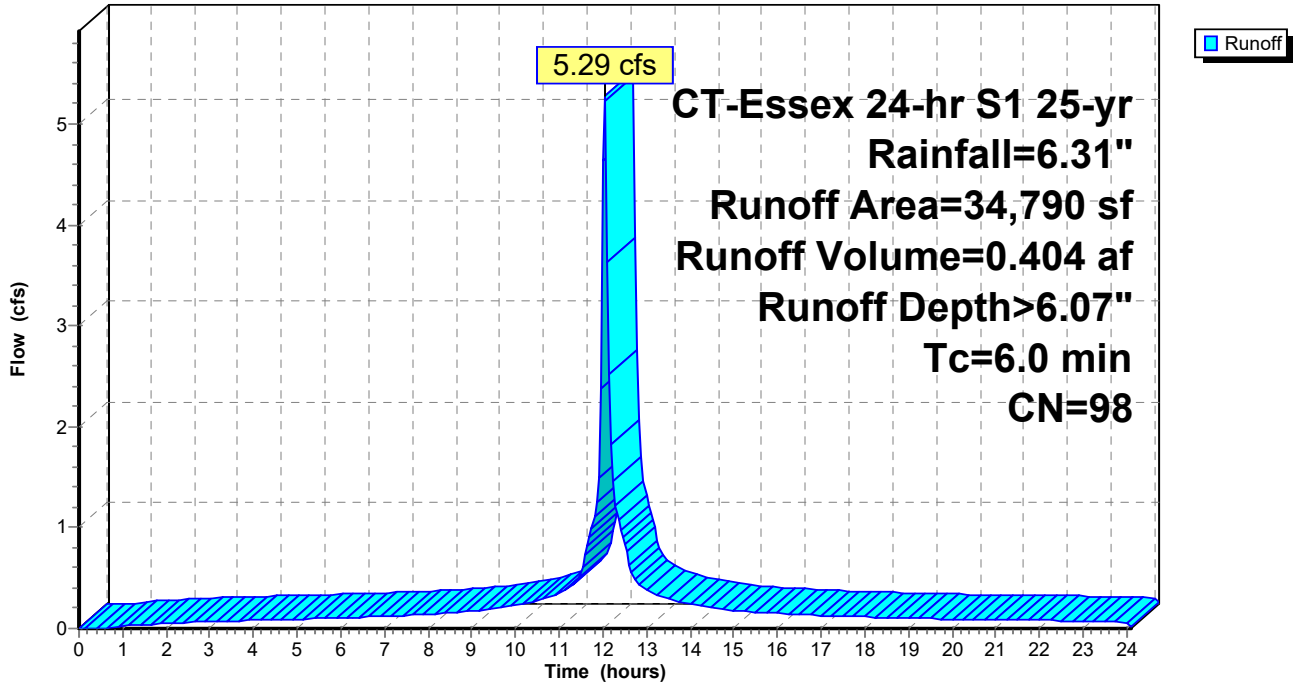
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.10 hrs, dt= 0.05 hrs  
 CT-Essex 24-hr S1 25-yr Rainfall=6.31"

Area (sf)	CN	Description
* 34,790	98	
34,790		100.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Subcatchment 20: DA 1**

Hydrograph



**Summary for Pond 25: SWL 1**

Inflow Area = 0.799 ac, 100.00% Impervious, Inflow Depth > 6.07" for 25-yr event  
 Inflow = 5.29 cfs @ 12.04 hrs, Volume= 0.404 af  
 Outflow = 1.93 cfs @ 12.20 hrs, Volume= 0.372 af, Atten= 63%, Lag= 9.7 min  
 Primary = 1.93 cfs @ 12.20 hrs, Volume= 0.372 af

Routing by Stor-Ind method, Time Span= 0.00-24.10 hrs, dt= 0.05 hrs  
 Starting Elev= 30.50' Storage= 1,650 cf  
 Peak Elev= 32.00' @ 12.20 hrs Storage= 7,096 cf (5,446 cf above start)

Plug-Flow detention time= 210.3 min calculated for 0.335 af (83% of inflow)  
 Center-of-Mass det. time= 84.6 min ( 829.6 - 745.0 )

Volume	Invert	Avail.Storage	Storage Description
#1	30.00'	16,231 cf	<b>Custom Stage Data</b> Listed below

Elevation (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
30.00	0	0
31.00	3,299	3,299
32.00	3,788	7,087
33.00	4,302	11,389
34.00	4,842	16,231

Device	Routing	Invert	Outlet Devices
#1	Primary	30.00'	<b>15.0" Round Culvert</b> L= 14.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 30.00' / 29.93' S= 0.0050 ' / ' Cc= 0.900 n= 0.012, Flow Area= 1.23 sf
#2	Device 1	30.50'	<b>30.0 deg x 2.33' rise Sharp-Crested Vee/Trap Weir</b> Cv= 2.61 (C= 3.26)

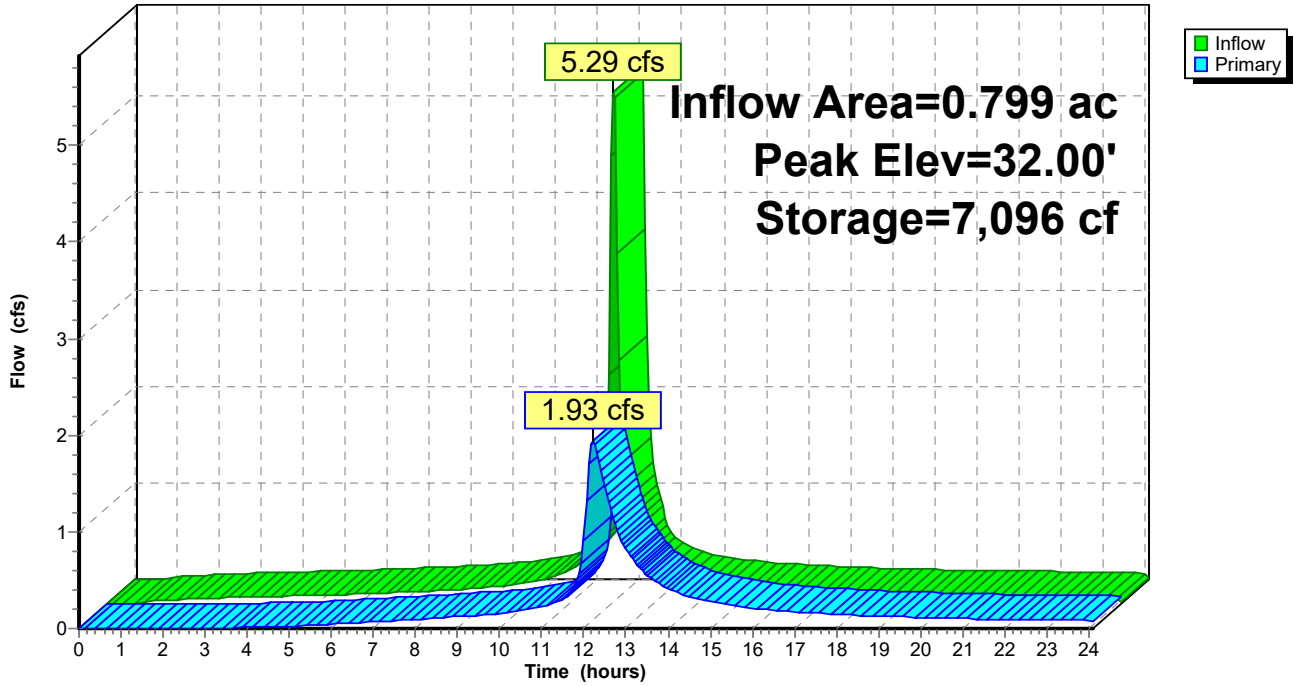
**Primary OutFlow** Max=1.93 cfs @ 12.20 hrs HW=32.00' (Free Discharge)

↑ **1=Culvert** (Passes 1.93 cfs of 6.70 cfs potential flow)

↑ **2=Sharp-Crested Vee/Trap Weir** (Weir Controls 1.93 cfs @ 3.20 fps)

**Pond 25: SWL 1**

Hydrograph



**20-50 SWL1**

*CT-Essex 24-hr S1 50-yr Rainfall=7.13"*

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Time span=0.00-24.10 hrs, dt=0.05 hrs, 483 points  
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN  
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

**Subcatchment20: DA 1**

Runoff Area=34,790 sf 100.00% Impervious Runoff Depth>6.89"  
Tc=6.0 min CN=98 Runoff=5.98 cfs 0.459 af

**Pond 25: SWL 1**

Peak Elev=32.10' Storage=7,537 cf Inflow=5.98 cfs 0.459 af  
Outflow=2.28 cfs 0.426 af

**Total Runoff Area = 0.799 ac Runoff Volume = 0.459 af Average Runoff Depth = 6.89"**  
**0.00% Pervious = 0.000 ac 100.00% Impervious = 0.799 ac**

**20-50 SWL1**

CT-Essex 24-hr S1 50-yr Rainfall=7.13"

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**Summary for Subcatchment 20: DA 1**

Runoff = 5.98 cfs @ 12.04 hrs, Volume= 0.459 af, Depth> 6.89"  
Routed to Pond 25 : SWL 1

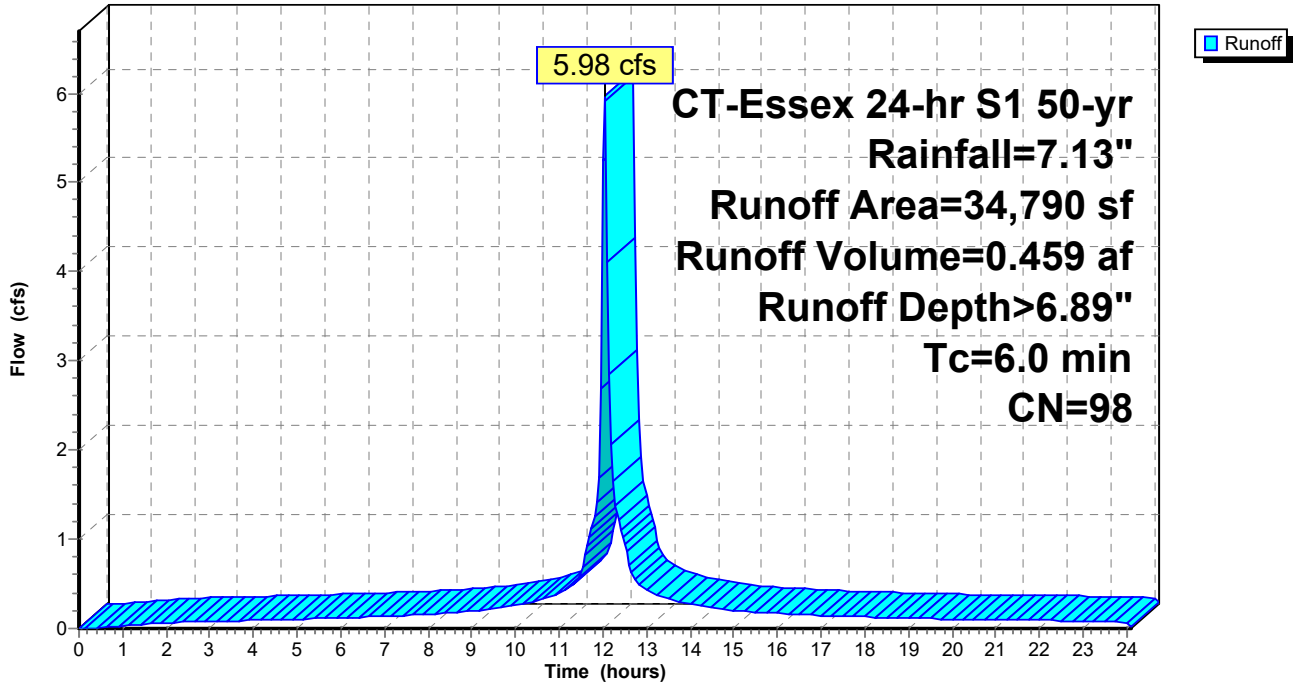
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.10 hrs, dt= 0.05 hrs  
CT-Essex 24-hr S1 50-yr Rainfall=7.13"

Area (sf)	CN	Description
* 34,790	98	
34,790		100.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Subcatchment 20: DA 1**

Hydrograph



**Summary for Pond 25: SWL 1**

Inflow Area = 0.799 ac, 100.00% Impervious, Inflow Depth > 6.89" for 50-yr event  
 Inflow = 5.98 cfs @ 12.04 hrs, Volume= 0.459 af  
 Outflow = 2.28 cfs @ 12.19 hrs, Volume= 0.426 af, Atten= 62%, Lag= 9.2 min  
 Primary = 2.28 cfs @ 12.19 hrs, Volume= 0.426 af

Routing by Stor-Ind method, Time Span= 0.00-24.10 hrs, dt= 0.05 hrs  
 Starting Elev= 30.50' Storage= 1,650 cf  
 Peak Elev= 32.10' @ 12.19 hrs Storage= 7,537 cf (5,887 cf above start)

Plug-Flow detention time= 196.3 min calculated for 0.387 af (84% of inflow)  
 Center-of-Mass det. time= 79.7 min ( 822.8 - 743.1 )

Volume	Invert	Avail.Storage	Storage Description
#1	30.00'	16,231 cf	<b>Custom Stage Data</b> Listed below

Elevation (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
30.00	0	0
31.00	3,299	3,299
32.00	3,788	7,087
33.00	4,302	11,389
34.00	4,842	16,231

Device	Routing	Invert	Outlet Devices
#1	Primary	30.00'	<b>15.0" Round Culvert</b> L= 14.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 30.00' / 29.93' S= 0.0050 ' / ' Cc= 0.900 n= 0.012, Flow Area= 1.23 sf
#2	Device 1	30.50'	<b>30.0 deg x 2.33' rise Sharp-Crested Vee/Trap Weir</b> Cv= 2.61 (C= 3.26)

**Primary OutFlow** Max=2.27 cfs @ 12.19 hrs HW=32.10' (Free Discharge)

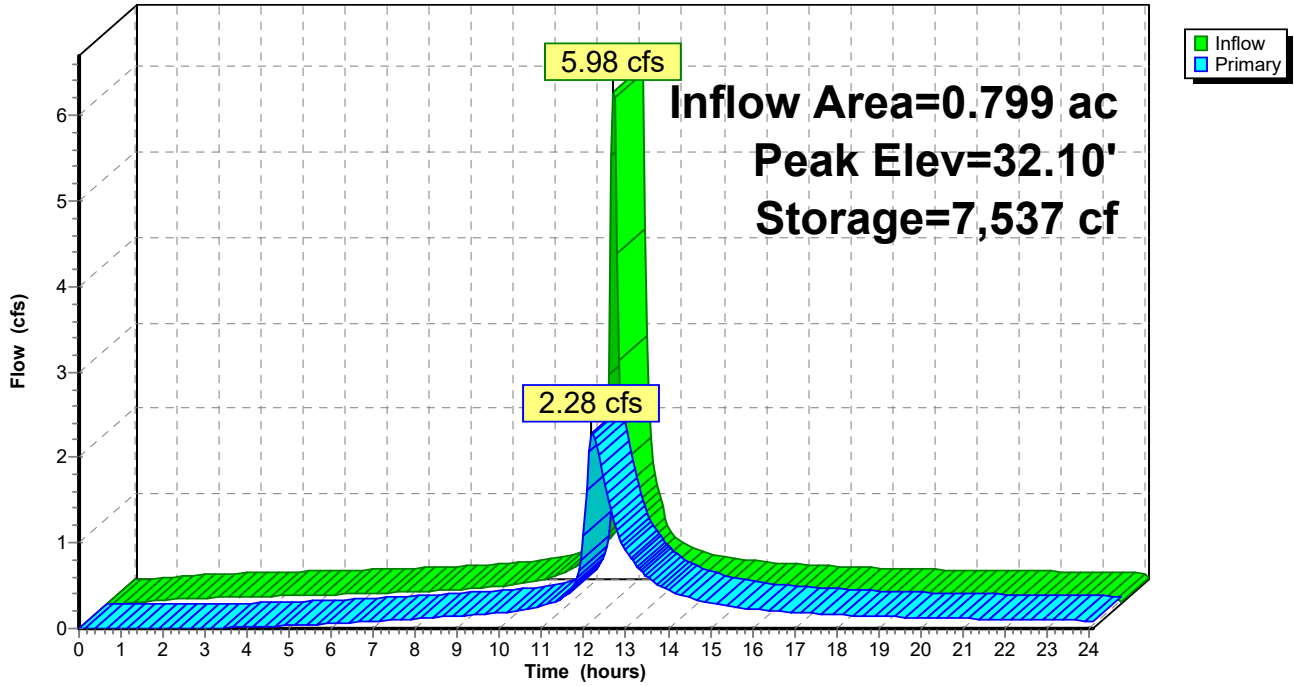
↑1=Culvert (Passes 2.27 cfs of 7.09 cfs potential flow)

↑2=Sharp-Crested Vee/Trap Weir (Weir Controls 2.27 cfs @ 3.30 fps)



### Pond 25: SWL 1

Hydrograph



**20-50 SWL1**

*CT-Essex 24-hr S1 100-yr Rainfall=8.01"*

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Time span=0.00-24.10 hrs, dt=0.05 hrs, 483 points  
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN  
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

**Subcatchment20: DA 1**

Runoff Area=34,790 sf 100.00% Impervious Runoff Depth>7.77"  
Tc=6.0 min CN=98 Runoff=6.70 cfs 0.517 af

**Pond 25: SWL 1**

Peak Elev=32.21' Storage=7,976 cf Inflow=6.70 cfs 0.517 af  
Outflow=2.66 cfs 0.483 af

**Total Runoff Area = 0.799 ac Runoff Volume = 0.517 af Average Runoff Depth = 7.77"**  
**0.00% Pervious = 0.000 ac 100.00% Impervious = 0.799 ac**

**20-50 SWL1**

CT-Essex 24-hr S1 100-yr Rainfall=8.01"

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**Summary for Subcatchment 20: DA 1**

Runoff = 6.70 cfs @ 12.04 hrs, Volume= 0.517 af, Depth> 7.77"  
Routed to Pond 25 : SWL 1

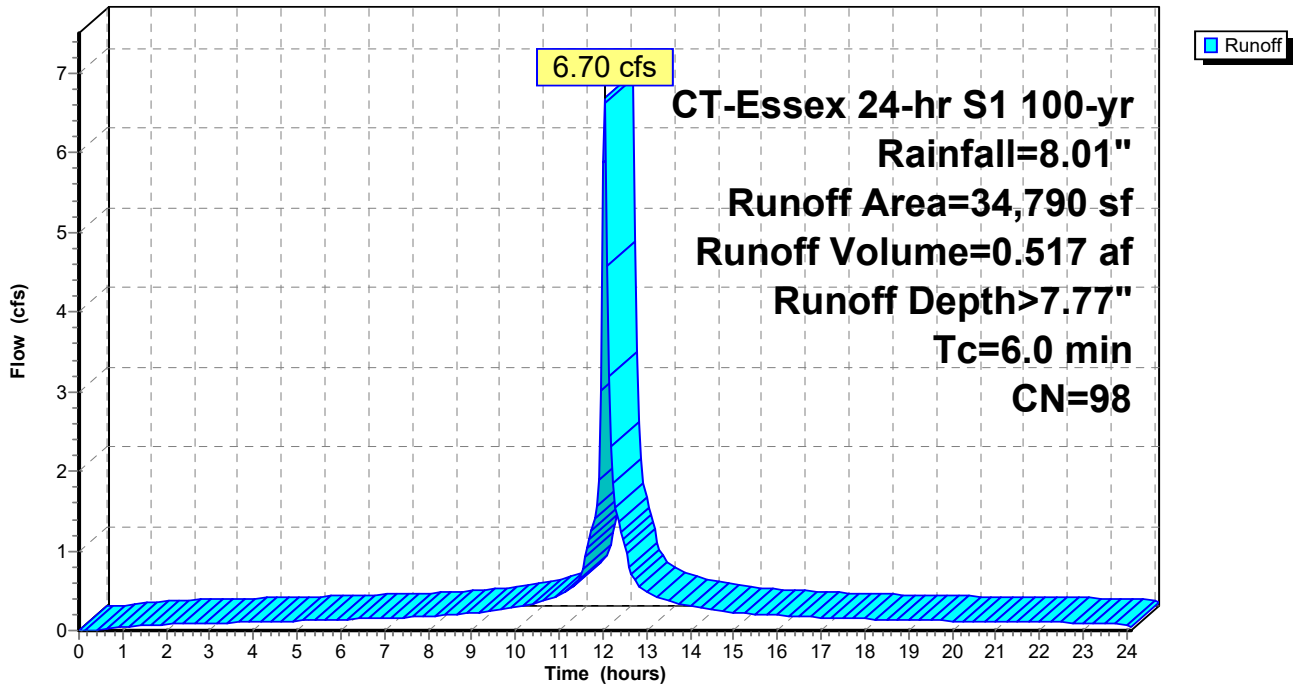
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.10 hrs, dt= 0.05 hrs  
CT-Essex 24-hr S1 100-yr Rainfall=8.01"

Area (sf)	CN	Description
* 34,790	98	
34,790		100.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Subcatchment 20: DA 1**

Hydrograph



**Summary for Pond 25: SWL 1**

Inflow Area = 0.799 ac, 100.00% Impervious, Inflow Depth > 7.77" for 100-yr event  
 Inflow = 6.70 cfs @ 12.04 hrs, Volume= 0.517 af  
 Outflow = 2.66 cfs @ 12.18 hrs, Volume= 0.483 af, Atten= 60%, Lag= 8.7 min  
 Primary = 2.66 cfs @ 12.18 hrs, Volume= 0.483 af

Routing by Stor-Ind method, Time Span= 0.00-24.10 hrs, dt= 0.05 hrs  
 Starting Elev= 30.50' Storage= 1,650 cf  
 Peak Elev= 32.21' @ 12.18 hrs Storage= 7,976 cf (6,326 cf above start)

Plug-Flow detention time= 184.9 min calculated for 0.445 af (86% of inflow)  
 Center-of-Mass det. time= 75.4 min ( 816.8 - 741.4 )

Volume	Invert	Avail.Storage	Storage Description
#1	30.00'	16,231 cf	<b>Custom Stage Data</b> Listed below

Elevation (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
30.00	0	0
31.00	3,299	3,299
32.00	3,788	7,087
33.00	4,302	11,389
34.00	4,842	16,231

Device	Routing	Invert	Outlet Devices
#1	Primary	30.00'	<b>15.0" Round Culvert</b> L= 14.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 30.00' / 29.93' S= 0.0050 '/ Cc= 0.900 n= 0.012, Flow Area= 1.23 sf
#2	Device 1	30.50'	<b>30.0 deg x 2.33' rise Sharp-Crested Vee/Trap Weir</b> Cv= 2.61 (C= 3.26)

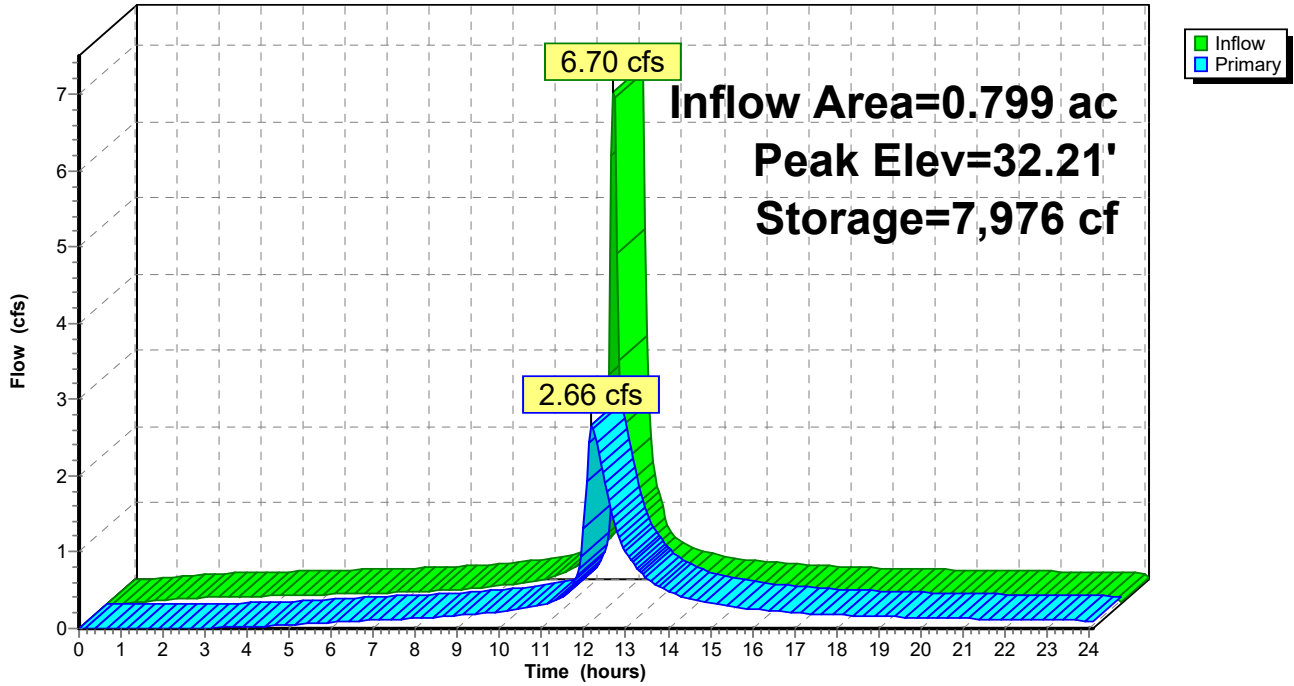
**Primary OutFlow** Max=2.65 cfs @ 12.18 hrs HW=32.20' (Free Discharge)

↑1=Culvert (Passes 2.65 cfs of 7.42 cfs potential flow)

↑2=Sharp-Crested Vee/Trap Weir (Weir Controls 2.65 cfs @ 3.41 fps)

**Pond 25: SWL 1**

Hydrograph



**20-50 SWL2**

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**Rainfall Events Listing (selected events)**

Event#	Event Name	Storm Type	Curve	Mode	Duration (hours)	B/B	Depth (inches)	AMC
1	2-yr	CT-Essex 24-hr S1	2-yr	Default	24.00	1	3.44	2
2	5-yr	CT-Essex 24-hr S1	5-yr	Default	24.00	1	4.41	2
3	10-yr	CT-Essex 24-hr S1	10-yr	Default	24.00	1	5.21	2
4	25-yr	CT-Essex 24-hr S1	25-yr	Default	24.00	1	6.31	2
5	50-yr	CT-Essex 24-hr S1	50-yr	Default	24.00	1	7.13	2
6	100-yr	CT-Essex 24-hr S1	100-yr	Default	24.00	1	8.01	2

**20-50 SWL2**

*CT-Essex 24-hr S1 2-yr Rainfall=3.44"*

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Time span=0.00-24.10 hrs, dt=0.05 hrs, 483 points  
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN  
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

**Subcatchment20: DA 2**

Runoff Area=48,685 sf 100.00% Impervious Runoff Depth>3.21"  
Tc=6.0 min CN=98 Runoff=4.05 cfs 0.299 af

**Pond 25: SWL 2**

Peak Elev=22.56' Storage=5,027 cf Inflow=4.05 cfs 0.299 af  
Outflow=0.93 cfs 0.375 af

**Total Runoff Area = 1.118 ac Runoff Volume = 0.299 af Average Runoff Depth = 3.21"**  
**0.00% Pervious = 0.000 ac 100.00% Impervious = 1.118 ac**

**20-50 SWL2**

CT-Essex 24-hr S1 2-yr Rainfall=3.44"

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**Summary for Subcatchment 20: DA 2**

Runoff = 4.05 cfs @ 12.04 hrs, Volume= 0.299 af, Depth> 3.21"  
Routed to Pond 25 : SWL 2

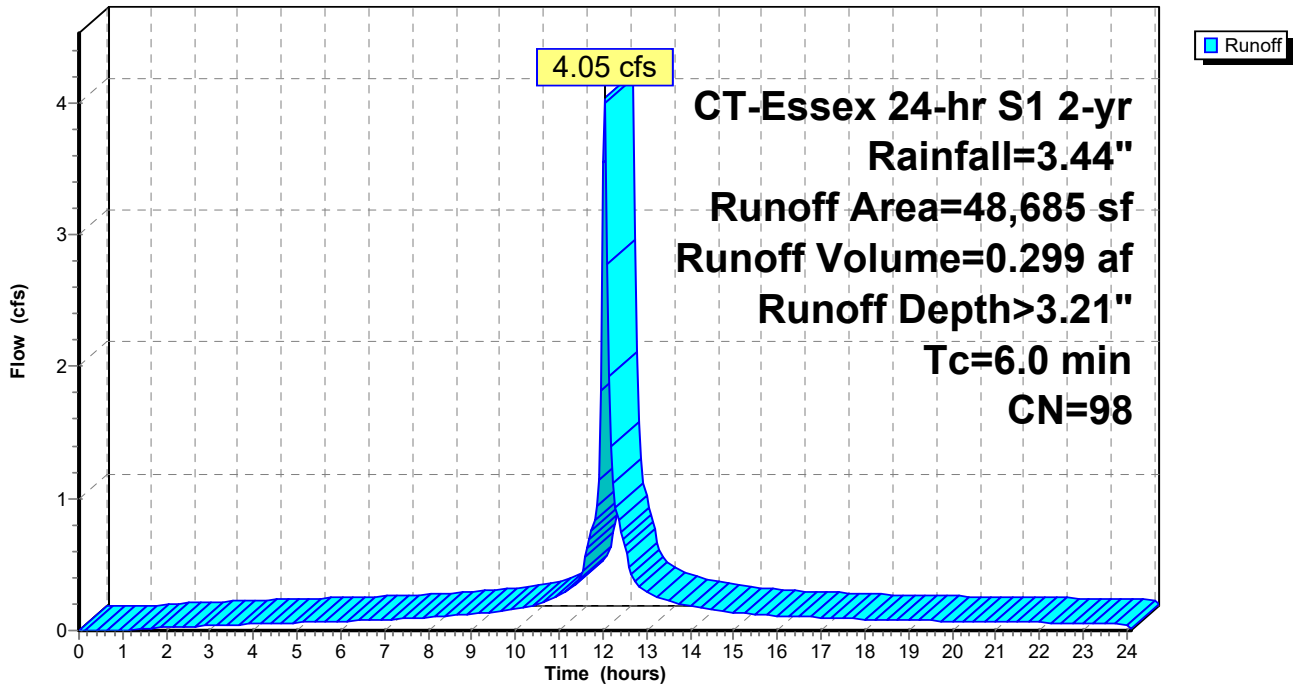
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.10 hrs, dt= 0.05 hrs  
CT-Essex 24-hr S1 2-yr Rainfall=3.44"

Area (sf)	CN	Description
* 48,685	98	
48,685		100.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Subcatchment 20: DA 2**

Hydrograph





**Summary for Pond 25: SWL 2**

Inflow Area = 1.118 ac, 100.00% Impervious, Inflow Depth > 3.21" for 2-yr event  
 Inflow = 4.05 cfs @ 12.04 hrs, Volume= 0.299 af  
 Outflow = 0.93 cfs @ 12.31 hrs, Volume= 0.375 af, Atten= 77%, Lag= 16.2 min  
 Primary = 0.93 cfs @ 12.31 hrs, Volume= 0.375 af

Routing by Stor-Ind method, Time Span= 0.00-24.10 hrs, dt= 0.05 hrs  
 Starting Elev= 22.50' Storage= 4,505 cf  
 Peak Elev= 22.56' @ 12.31 hrs Storage= 5,027 cf (522 cf above start)

Plug-Flow detention time= 164.8 min calculated for 0.271 af (91% of inflow)  
 Center-of-Mass det. time= (not calculated: outflow precedes inflow)

Volume	Invert	Avail.Storage	Storage Description
#1	22.00'	29,613 cf	<b>Custom Stage Data</b> Listed below

Elevation (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
22.00	0	0
23.00	9,010	9,010
24.00	9,863	18,873
25.00	10,740	29,613

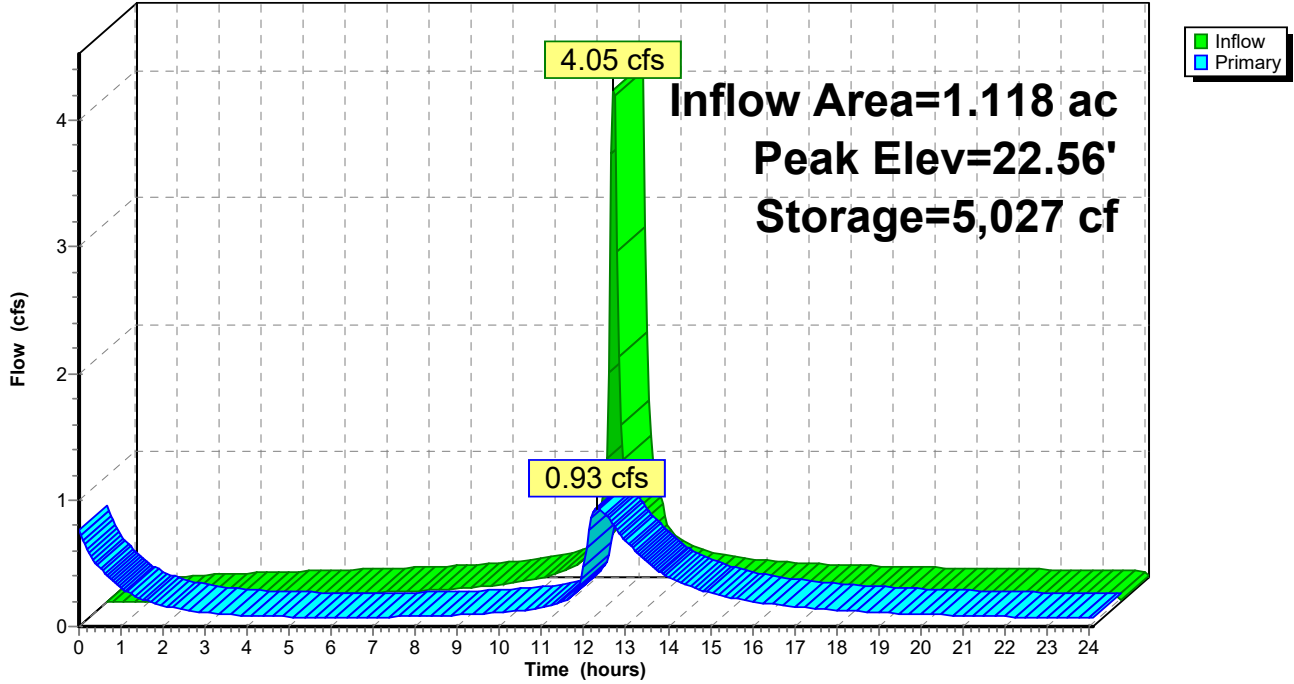
Device	Routing	Invert	Outlet Devices
#1	Primary	22.00'	<b>15.0" Round Culvert</b> L= 8.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 22.00' / 21.96' S= 0.0050 ' S= 0.0050 ' Cc= 0.900 n= 0.012, Flow Area= 1.23 sf
#2	Primary	22.50'	<b>30.0 deg x 1.33' rise Sharp-Crested Vee/Trap Weir</b> Cv= 2.61 (C= 3.26)

**Primary OutFlow** Max=0.93 cfs @ 12.31 hrs HW=22.56' (Free Discharge)

- 1=Culvert (Barrel Controls 0.93 cfs @ 2.58 fps)
- 2=Sharp-Crested Vee/Trap Weir (Weir Controls 0.00 cfs @ 0.63 fps)

### Pond 25: SWL 2

Hydrograph



**20-50 SWL2**

*CT-Essex 24-hr S1 5-yr Rainfall=4.41"*

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Time span=0.00-24.10 hrs, dt=0.05 hrs, 483 points  
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN  
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

**Subcatchment20: DA 2**

Runoff Area=48,685 sf 100.00% Impervious Runoff Depth>4.17"  
Tc=6.0 min CN=98 Runoff=5.18 cfs 0.389 af

**Pond 25: SWL 2**

Peak Elev=22.67' Storage=6,049 cf Inflow=5.18 cfs 0.389 af  
Outflow=1.31 cfs 0.462 af

**Total Runoff Area = 1.118 ac Runoff Volume = 0.389 af Average Runoff Depth = 4.17"**  
**0.00% Pervious = 0.000 ac 100.00% Impervious = 1.118 ac**

**20-50 SWL2**

CT-Essex 24-hr S1 5-yr Rainfall=4.41"

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**Summary for Subcatchment 20: DA 2**

Runoff = 5.18 cfs @ 12.04 hrs, Volume= 0.389 af, Depth> 4.17"  
Routed to Pond 25 : SWL 2

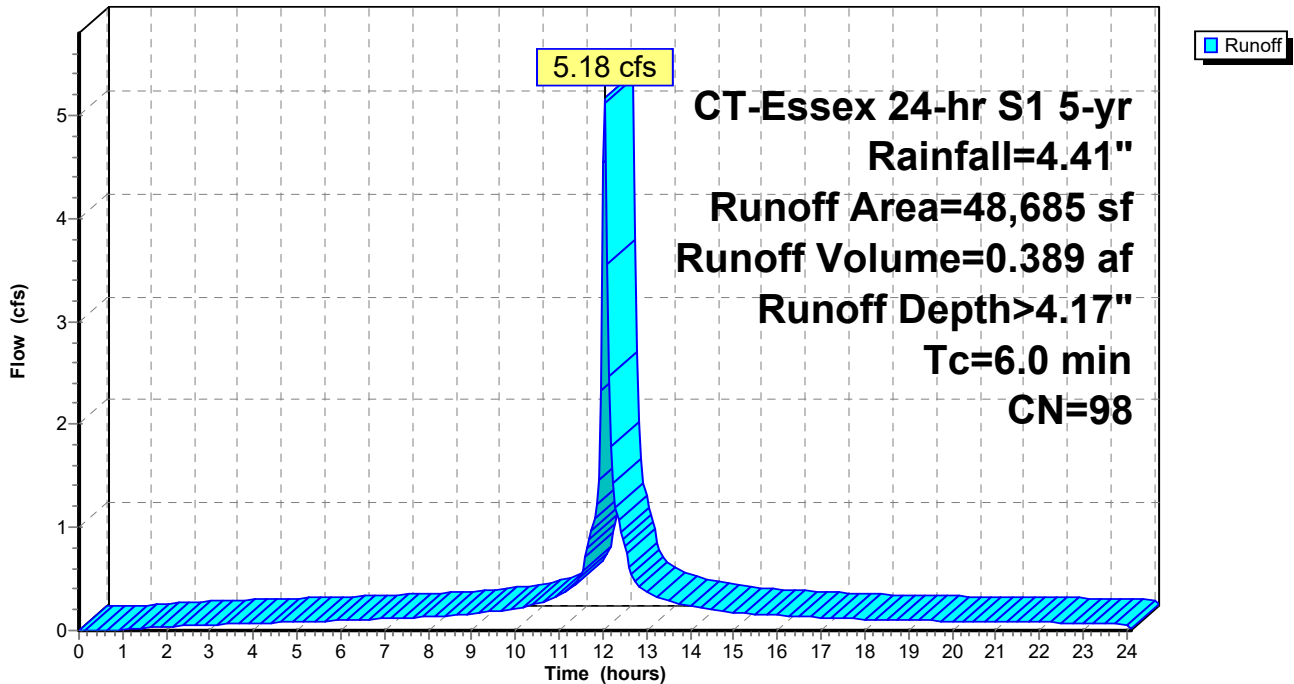
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.10 hrs, dt= 0.05 hrs  
CT-Essex 24-hr S1 5-yr Rainfall=4.41"

Area (sf)	CN	Description
* 48,685	98	
48,685		100.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Subcatchment 20: DA 2**

Hydrograph



**Summary for Pond 25: SWL 2**

Inflow Area = 1.118 ac, 100.00% Impervious, Inflow Depth > 4.17" for 5-yr event  
 Inflow = 5.18 cfs @ 12.04 hrs, Volume= 0.389 af  
 Outflow = 1.31 cfs @ 12.28 hrs, Volume= 0.462 af, Atten= 75%, Lag= 14.3 min  
 Primary = 1.31 cfs @ 12.28 hrs, Volume= 0.462 af

Routing by Stor-Ind method, Time Span= 0.00-24.10 hrs, dt= 0.05 hrs  
 Starting Elev= 22.50' Storage= 4,505 cf  
 Peak Elev= 22.67' @ 12.28 hrs Storage= 6,049 cf (1,544 cf above start)

Plug-Flow detention time= 148.2 min calculated for 0.357 af (92% of inflow)  
 Center-of-Mass det. time= (not calculated: outflow precedes inflow)

Volume	Invert	Avail.Storage	Storage Description
#1	22.00'	29,613 cf	<b>Custom Stage Data</b> Listed below

Elevation (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
22.00	0	0
23.00	9,010	9,010
24.00	9,863	18,873
25.00	10,740	29,613

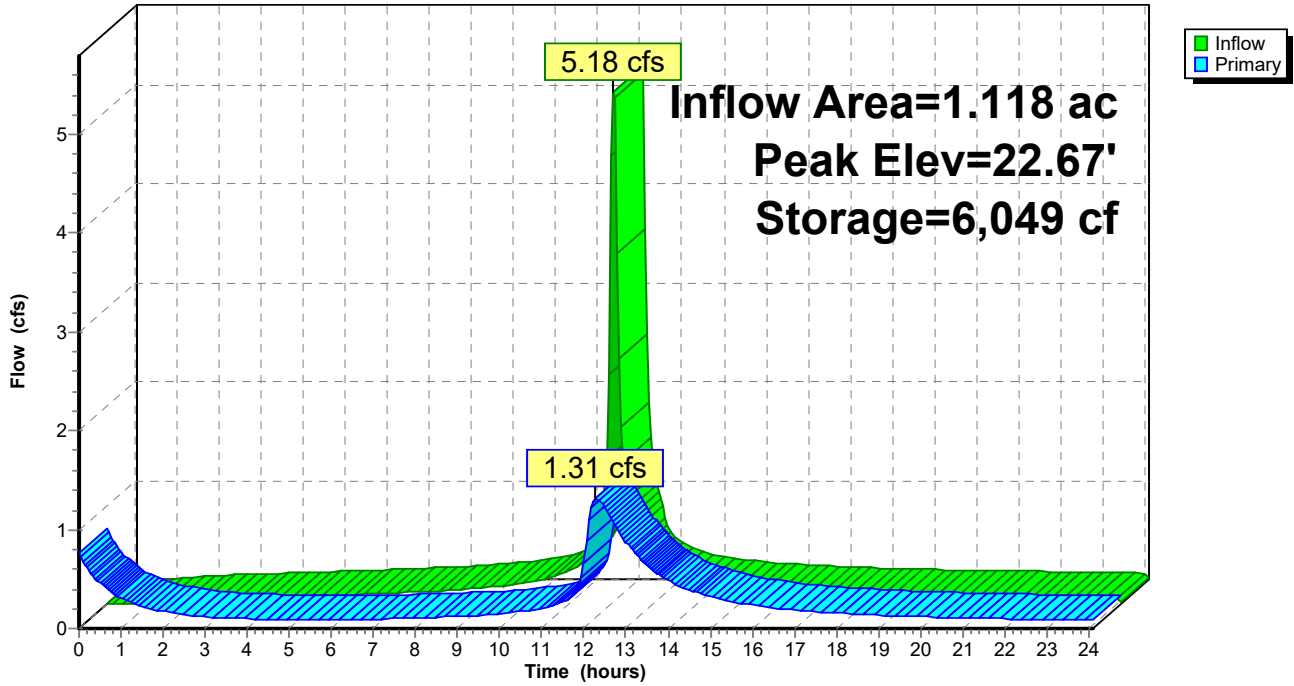
Device	Routing	Invert	Outlet Devices
#1	Primary	22.00'	<b>15.0" Round Culvert</b> L= 8.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 22.00' / 21.96' S= 0.0050 ' S= 0.0050 ' Cc= 0.900 n= 0.012, Flow Area= 1.23 sf
#2	Primary	22.50'	<b>30.0 deg x 1.33' rise Sharp-Crested Vee/Trap Weir</b> Cv= 2.61 (C= 3.26)

**Primary OutFlow** Max=1.31 cfs @ 12.28 hrs HW=22.67' (Free Discharge)

- 1=Culvert (Barrel Controls 1.30 cfs @ 2.81 fps)
- 2=Sharp-Crested Vee/Trap Weir (Weir Controls 0.01 cfs @ 1.08 fps)

### Pond 25: SWL 2

Hydrograph



**20-50 SWL2**

*CT-Essex 24-hr S1 10-yr Rainfall=5.21"*

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Time span=0.00-24.10 hrs, dt=0.05 hrs, 483 points  
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN  
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

**Subcatchment20: DA 2**

Runoff Area=48,685 sf 100.00% Impervious Runoff Depth>4.97"  
Tc=6.0 min CN=98 Runoff=6.12 cfs 0.463 af

**Pond 25: SWL 2**

Peak Elev=22.76' Storage=6,845 cf Inflow=6.12 cfs 0.463 af  
Outflow=1.65 cfs 0.533 af

**Total Runoff Area = 1.118 ac Runoff Volume = 0.463 af Average Runoff Depth = 4.97"**  
**0.00% Pervious = 0.000 ac 100.00% Impervious = 1.118 ac**

**20-50 SWL2**

CT-Essex 24-hr S1 10-yr Rainfall=5.21"

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**Summary for Subcatchment 20: DA 2**

Runoff = 6.12 cfs @ 12.04 hrs, Volume= 0.463 af, Depth> 4.97"  
Routed to Pond 25 : SWL 2

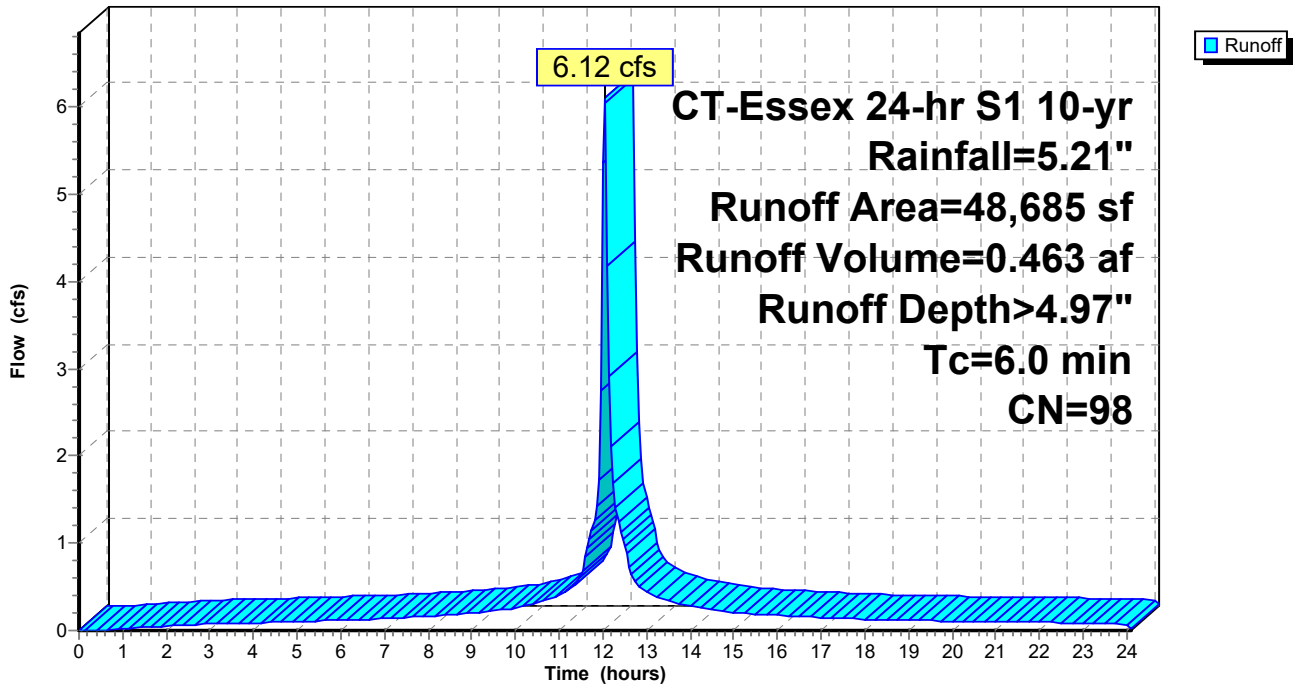
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.10 hrs, dt= 0.05 hrs  
CT-Essex 24-hr S1 10-yr Rainfall=5.21"

Area (sf)	CN	Description
* 48,685	98	
48,685		100.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Subcatchment 20: DA 2**

Hydrograph





**Summary for Pond 25: SWL 2**

Inflow Area = 1.118 ac, 100.00% Impervious, Inflow Depth > 4.97" for 10-yr event  
 Inflow = 6.12 cfs @ 12.04 hrs, Volume= 0.463 af  
 Outflow = 1.65 cfs @ 12.26 hrs, Volume= 0.533 af, Atten= 73%, Lag= 13.4 min  
 Primary = 1.65 cfs @ 12.26 hrs, Volume= 0.533 af

Routing by Stor-Ind method, Time Span= 0.00-24.10 hrs, dt= 0.05 hrs  
 Starting Elev= 22.50' Storage= 4,505 cf  
 Peak Elev= 22.76' @ 12.26 hrs Storage= 6,845 cf (2,340 cf above start)

Plug-Flow detention time= 138.0 min calculated for 0.429 af (93% of inflow)  
 Center-of-Mass det. time= (not calculated: outflow precedes inflow)

Volume	Invert	Avail.Storage	Storage Description
#1	22.00'	29,613 cf	<b>Custom Stage Data</b> Listed below

Elevation (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
22.00	0	0
23.00	9,010	9,010
24.00	9,863	18,873
25.00	10,740	29,613

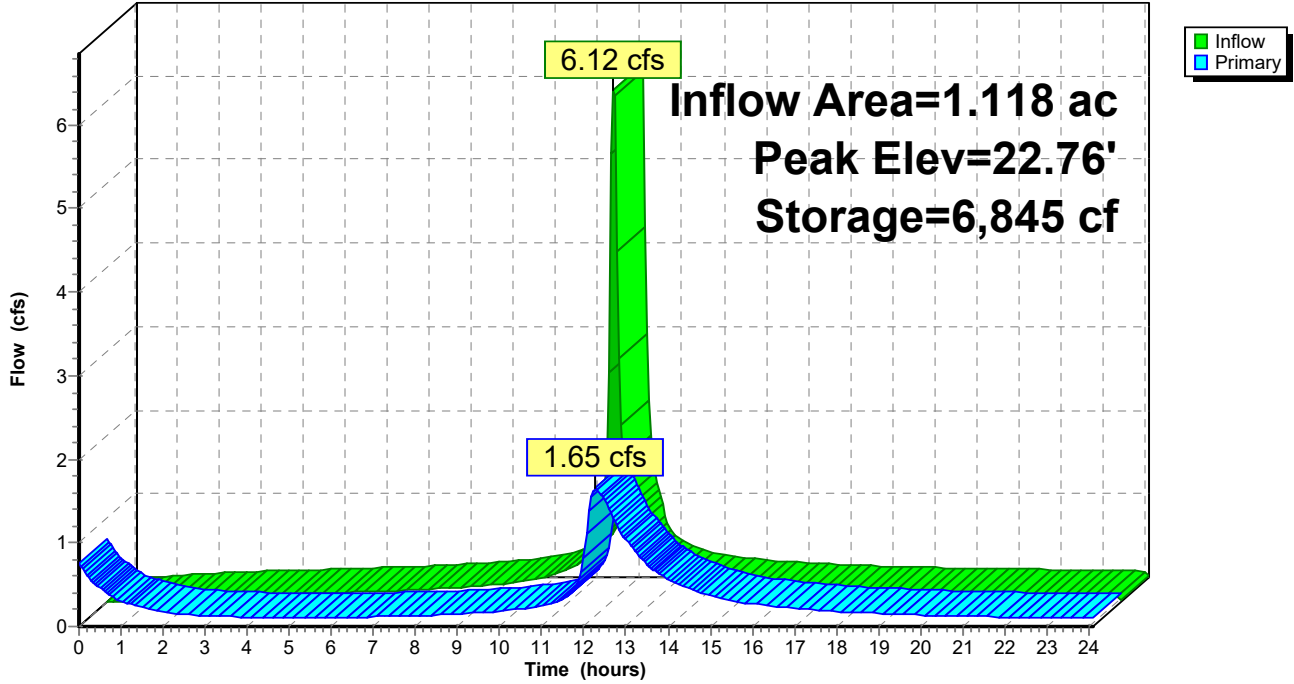
Device	Routing	Invert	Outlet Devices
#1	Primary	22.00'	<b>15.0" Round Culvert</b> L= 8.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 22.00' / 21.96' S= 0.0050 ' S= 0.0050 ' Cc= 0.900 n= 0.012, Flow Area= 1.23 sf
#2	Primary	22.50'	<b>30.0 deg x 1.33' rise Sharp-Crested Vee/Trap Weir</b> Cv= 2.61 (C= 3.26)

**Primary OutFlow** Max=1.64 cfs @ 12.26 hrs HW=22.76' (Free Discharge)

- 1=Culvert (Barrel Controls 1.62 cfs @ 2.97 fps)
- 2=Sharp-Crested Vee/Trap Weir (Weir Controls 0.02 cfs @ 1.33 fps)

Pond 25: SWL 2

Hydrograph



**20-50 SWL2**

CT-Essex 24-hr S1 25-yr Rainfall=6.31"

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Time span=0.00-24.10 hrs, dt=0.05 hrs, 483 points  
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN  
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

**Subcatchment20: DA 2**

Runoff Area=48,685 sf 100.00% Impervious Runoff Depth>6.07"  
Tc=6.0 min CN=98 Runoff=7.41 cfs 0.565 af

**Pond 25: SWL 2**

Peak Elev=22.88' Storage=7,891 cf Inflow=7.41 cfs 0.565 af  
Outflow=2.14 cfs 0.633 af

**Total Runoff Area = 1.118 ac Runoff Volume = 0.565 af Average Runoff Depth = 6.07"**  
**0.00% Pervious = 0.000 ac 100.00% Impervious = 1.118 ac**

**20-50 SWL2**

CT-Essex 24-hr S1 25-yr Rainfall=6.31"

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**Summary for Subcatchment 20: DA 2**

Runoff = 7.41 cfs @ 12.04 hrs, Volume= 0.565 af, Depth> 6.07"

Routed to Pond 25 : SWL 2

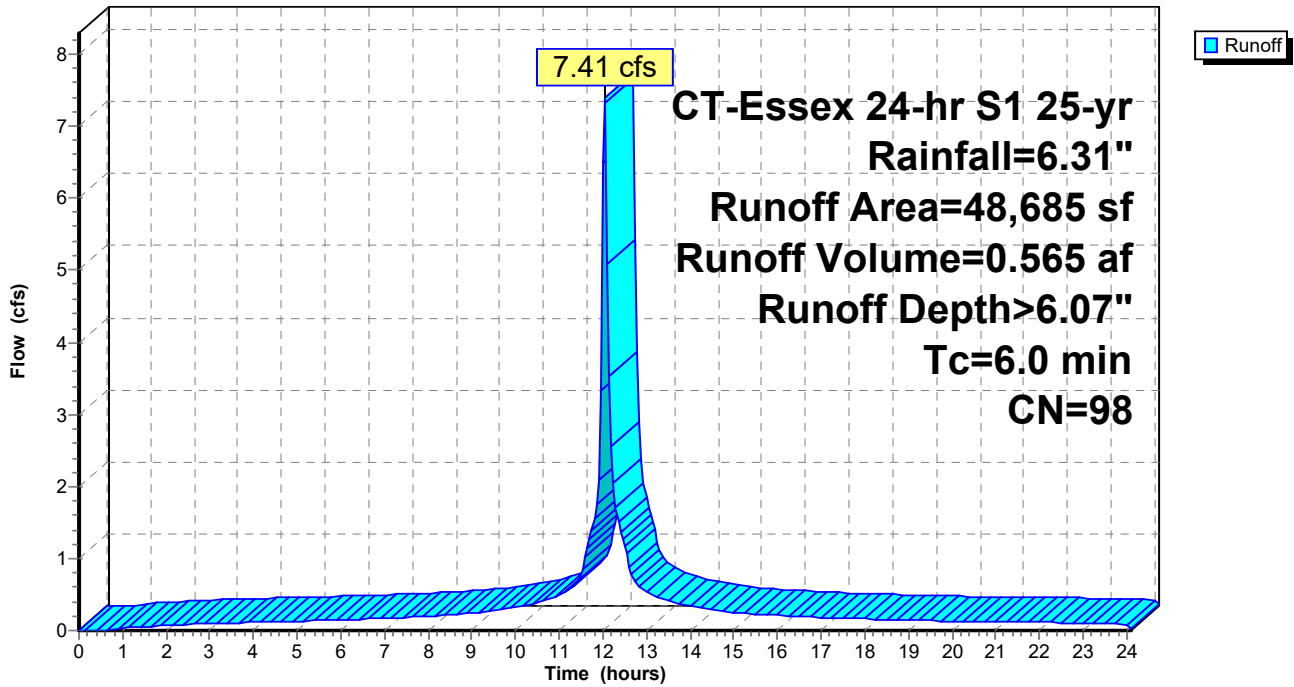
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.10 hrs, dt= 0.05 hrs  
CT-Essex 24-hr S1 25-yr Rainfall=6.31"

Area (sf)	CN	Description
* 48,685	98	
48,685		100.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Subcatchment 20: DA 2**

Hydrograph



**Summary for Pond 25: SWL 2**

Inflow Area = 1.118 ac, 100.00% Impervious, Inflow Depth > 6.07" for 25-yr event  
 Inflow = 7.41 cfs @ 12.04 hrs, Volume= 0.565 af  
 Outflow = 2.14 cfs @ 12.25 hrs, Volume= 0.633 af, Atten= 71%, Lag= 12.4 min  
 Primary = 2.14 cfs @ 12.25 hrs, Volume= 0.633 af

Routing by Stor-Ind method, Time Span= 0.00-24.10 hrs, dt= 0.05 hrs  
 Starting Elev= 22.50' Storage= 4,505 cf  
 Peak Elev= 22.88' @ 12.25 hrs Storage= 7,891 cf (3,386 cf above start)

Plug-Flow detention time= 126.8 min calculated for 0.528 af (93% of inflow)  
 Center-of-Mass det. time= (not calculated: outflow precedes inflow)

Volume	Invert	Avail.Storage	Storage Description
#1	22.00'	29,613 cf	<b>Custom Stage Data</b> Listed below

Elevation (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
22.00	0	0
23.00	9,010	9,010
24.00	9,863	18,873
25.00	10,740	29,613

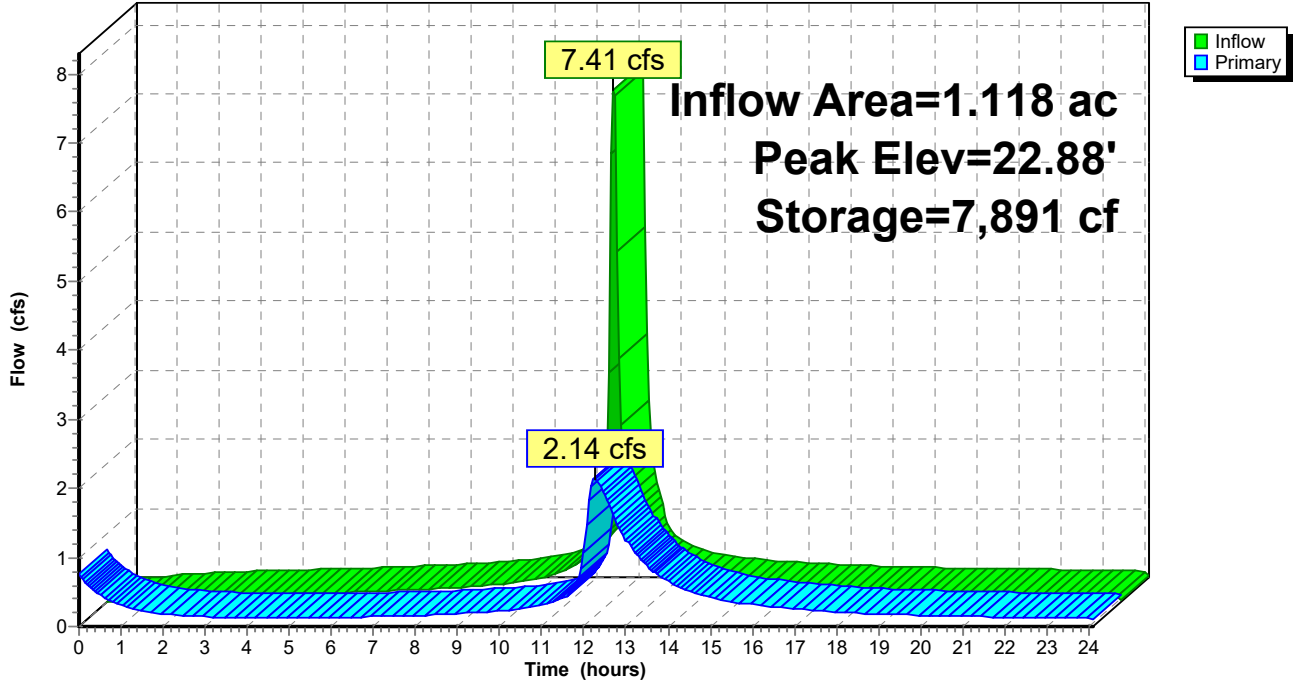
Device	Routing	Invert	Outlet Devices
#1	Primary	22.00'	<b>15.0" Round Culvert</b> L= 8.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 22.00' / 21.96' S= 0.0050 ' S= 0.0050 ' Cc= 0.900 n= 0.012, Flow Area= 1.23 sf
#2	Primary	22.50'	<b>30.0 deg x 1.33' rise Sharp-Crested Vee/Trap Weir</b> Cv= 2.61 (C= 3.26)

**Primary OutFlow** Max=2.13 cfs @ 12.25 hrs HW=22.88' (Free Discharge)

- 1=Culvert (Barrel Controls 2.07 cfs @ 3.18 fps)
- 2=Sharp-Crested Vee/Trap Weir (Weir Controls 0.06 cfs @ 1.60 fps)

**Pond 25: SWL 2**

Hydrograph



**20-50 SWL2**

*CT-Essex 24-hr S1 50-yr Rainfall=7.13"*

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Time span=0.00-24.10 hrs, dt=0.05 hrs, 483 points  
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN  
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

**Subcatchment20: DA 2**

Runoff Area=48,685 sf 100.00% Impervious Runoff Depth>6.89"  
Tc=6.0 min CN=98 Runoff=8.37 cfs 0.642 af

**Pond 25: SWL 2**

Peak Elev=22.96' Storage=8,633 cf Inflow=8.37 cfs 0.642 af  
Outflow=2.52 cfs 0.707 af

**Total Runoff Area = 1.118 ac Runoff Volume = 0.642 af Average Runoff Depth = 6.89"**  
**0.00% Pervious = 0.000 ac 100.00% Impervious = 1.118 ac**

**20-50 SWL2**

CT-Essex 24-hr S1 50-yr Rainfall=7.13"

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**Summary for Subcatchment 20: DA 2**

Runoff = 8.37 cfs @ 12.04 hrs, Volume= 0.642 af, Depth> 6.89"  
Routed to Pond 25 : SWL 2

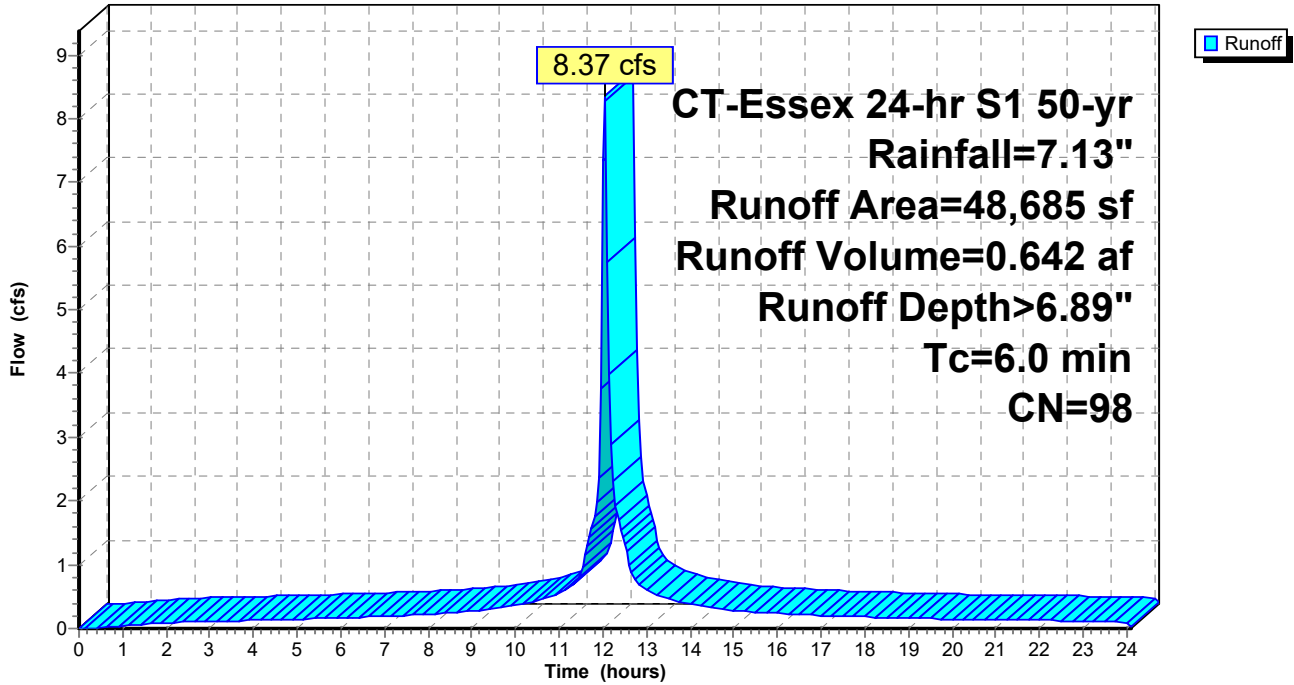
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.10 hrs, dt= 0.05 hrs  
CT-Essex 24-hr S1 50-yr Rainfall=7.13"

Area (sf)	CN	Description
* 48,685	98	
48,685		100.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Subcatchment 20: DA 2**

Hydrograph





**Summary for Pond 25: SWL 2**

Inflow Area = 1.118 ac, 100.00% Impervious, Inflow Depth > 6.89" for 50-yr event  
 Inflow = 8.37 cfs @ 12.04 hrs, Volume= 0.642 af  
 Outflow = 2.52 cfs @ 12.23 hrs, Volume= 0.707 af, Atten= 70%, Lag= 11.8 min  
 Primary = 2.52 cfs @ 12.23 hrs, Volume= 0.707 af

Routing by Stor-Ind method, Time Span= 0.00-24.10 hrs, dt= 0.05 hrs  
 Starting Elev= 22.50' Storage= 4,505 cf  
 Peak Elev= 22.96' @ 12.23 hrs Storage= 8,633 cf (4,128 cf above start)

Plug-Flow detention time= 120.5 min calculated for 0.603 af (94% of inflow)  
 Center-of-Mass det. time= (not calculated: outflow precedes inflow)

Volume	Invert	Avail.Storage	Storage Description
#1	22.00'	29,613 cf	<b>Custom Stage Data</b> Listed below

Elevation (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
22.00	0	0
23.00	9,010	9,010
24.00	9,863	18,873
25.00	10,740	29,613

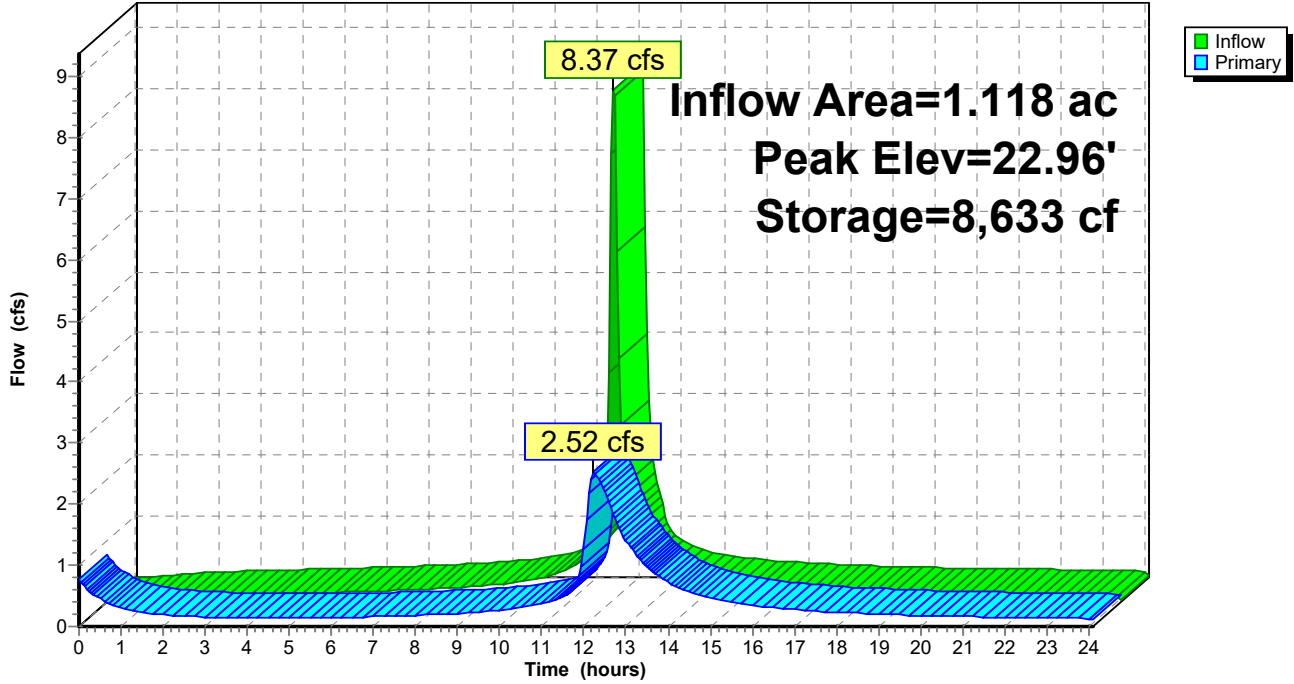
Device	Routing	Invert	Outlet Devices
#1	Primary	22.00'	<b>15.0" Round Culvert</b> L= 8.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 22.00' / 21.96' S= 0.0050 ' S= 0.0050 ' Cc= 0.900 n= 0.012, Flow Area= 1.23 sf
#2	Primary	22.50'	<b>30.0 deg x 1.33' rise Sharp-Crested Vee/Trap Weir</b> Cv= 2.61 (C= 3.26)

**Primary OutFlow** Max=2.51 cfs @ 12.23 hrs HW=22.96' (Free Discharge)

- 1=Culvert (Barrel Controls 2.41 cfs @ 3.31 fps)
- 2=Sharp-Crested Vee/Trap Weir (Weir Controls 0.10 cfs @ 1.76 fps)

Pond 25: SWL 2

Hydrograph



**20-50 SWL2**

*CT-Essex 24-hr S1 100-yr Rainfall=8.01"*

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Time span=0.00-24.10 hrs, dt=0.05 hrs, 483 points  
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN  
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

**Subcatchment20: DA 2**

Runoff Area=48,685 sf 100.00% Impervious Runoff Depth>7.77"  
Tc=6.0 min CN=98 Runoff=9.38 cfs 0.724 af

**Pond 25: SWL 2**

Peak Elev=23.04' Storage=9,389 cf Inflow=9.38 cfs 0.724 af  
Outflow=2.91 cfs 0.786 af

**Total Runoff Area = 1.118 ac Runoff Volume = 0.724 af Average Runoff Depth = 7.77"**  
**0.00% Pervious = 0.000 ac 100.00% Impervious = 1.118 ac**

**20-50 SWL2**

CT-Essex 24-hr S1 100-yr Rainfall=8.01"

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**Summary for Subcatchment 20: DA 2**

Runoff = 9.38 cfs @ 12.04 hrs, Volume= 0.724 af, Depth> 7.77"  
Routed to Pond 25 : SWL 2

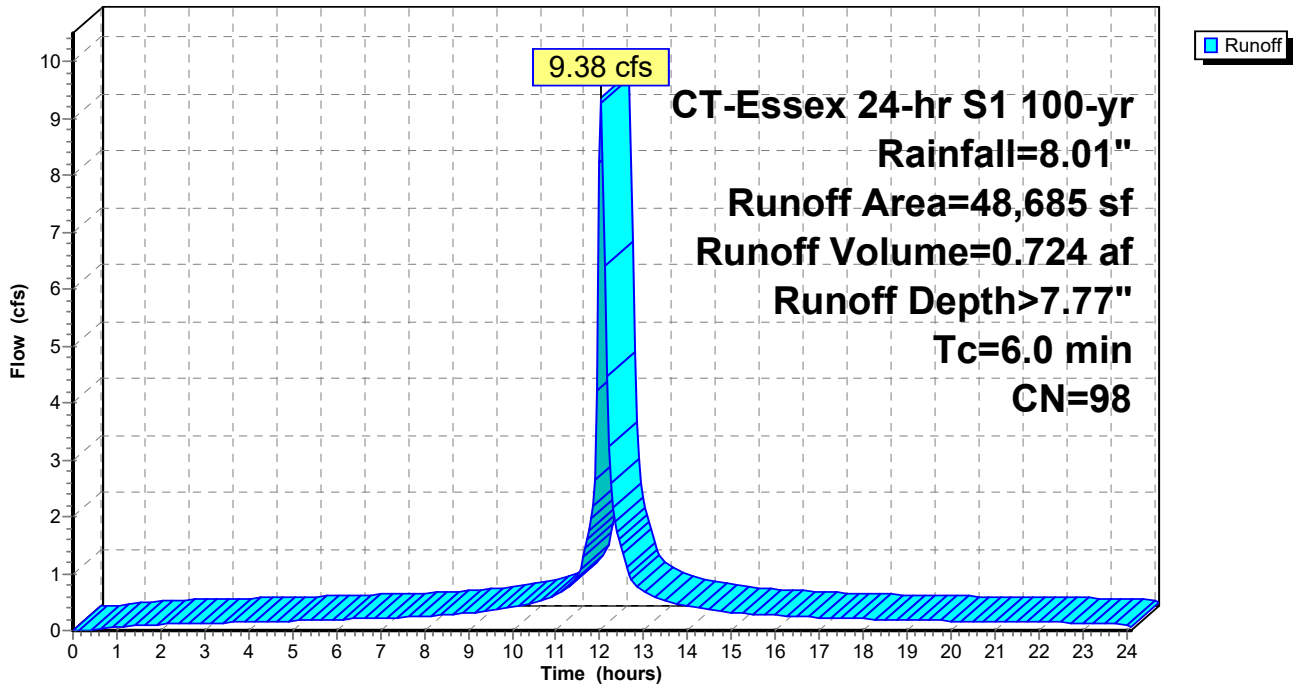
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.10 hrs, dt= 0.05 hrs  
CT-Essex 24-hr S1 100-yr Rainfall=8.01"

Area (sf)	CN	Description
* 48,685	98	
48,685		100.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Subcatchment 20: DA 2**

Hydrograph



**20-50 SWL2**

CT-Essex 24-hr S1 100-yr Rainfall=8.01"

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**Summary for Pond 25: SWL 2**

Inflow Area = 1.118 ac, 100.00% Impervious, Inflow Depth > 7.77" for 100-yr event  
 Inflow = 9.38 cfs @ 12.04 hrs, Volume= 0.724 af  
 Outflow = 2.91 cfs @ 12.23 hrs, Volume= 0.786 af, Atten= 69%, Lag= 11.2 min  
 Primary = 2.91 cfs @ 12.23 hrs, Volume= 0.786 af

Routing by Stor-Ind method, Time Span= 0.00-24.10 hrs, dt= 0.05 hrs  
 Starting Elev= 22.50' Storage= 4,505 cf  
 Peak Elev= 23.04' @ 12.23 hrs Storage= 9,389 cf (4,884 cf above start)

Plug-Flow detention time= 114.4 min calculated for 0.681 af (94% of inflow)  
 Center-of-Mass det. time= (not calculated: outflow precedes inflow)

Volume	Invert	Avail.Storage	Storage Description
#1	22.00'	29,613 cf	<b>Custom Stage Data</b> Listed below

Elevation (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
22.00	0	0
23.00	9,010	9,010
24.00	9,863	18,873
25.00	10,740	29,613

Device	Routing	Invert	Outlet Devices
#1	Primary	22.00'	<b>15.0" Round Culvert</b> L= 8.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 22.00' / 21.96' S= 0.0050 '/' Cc= 0.900 n= 0.012, Flow Area= 1.23 sf
#2	Primary	22.50'	<b>30.0 deg x 1.33' rise Sharp-Crested Vee/Trap Weir</b> Cv= 2.61 (C= 3.26)

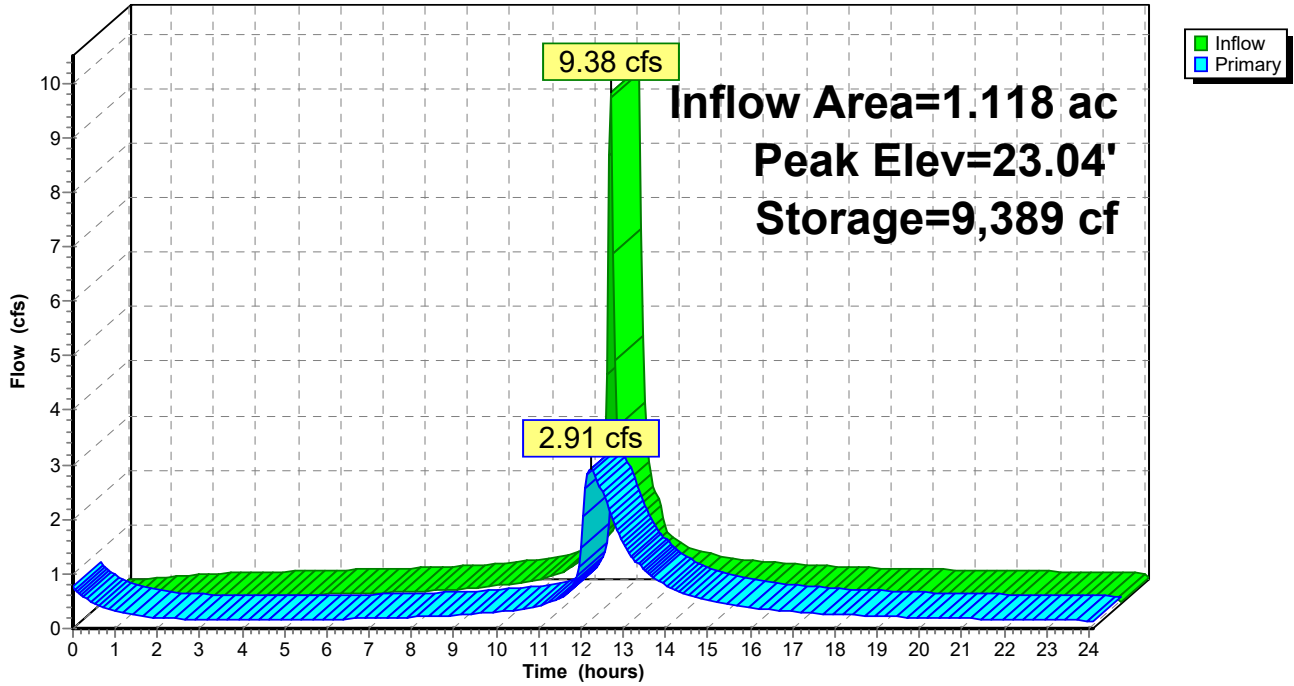
**Primary OutFlow** Max=2.90 cfs @ 12.23 hrs HW=23.04' (Free Discharge)

1=Culvert (Barrel Controls 2.76 cfs @ 3.43 fps)

2=Sharp-Crested Vee/Trap Weir (Weir Controls 0.15 cfs @ 1.91 fps)

**Pond 25: SWL 2**

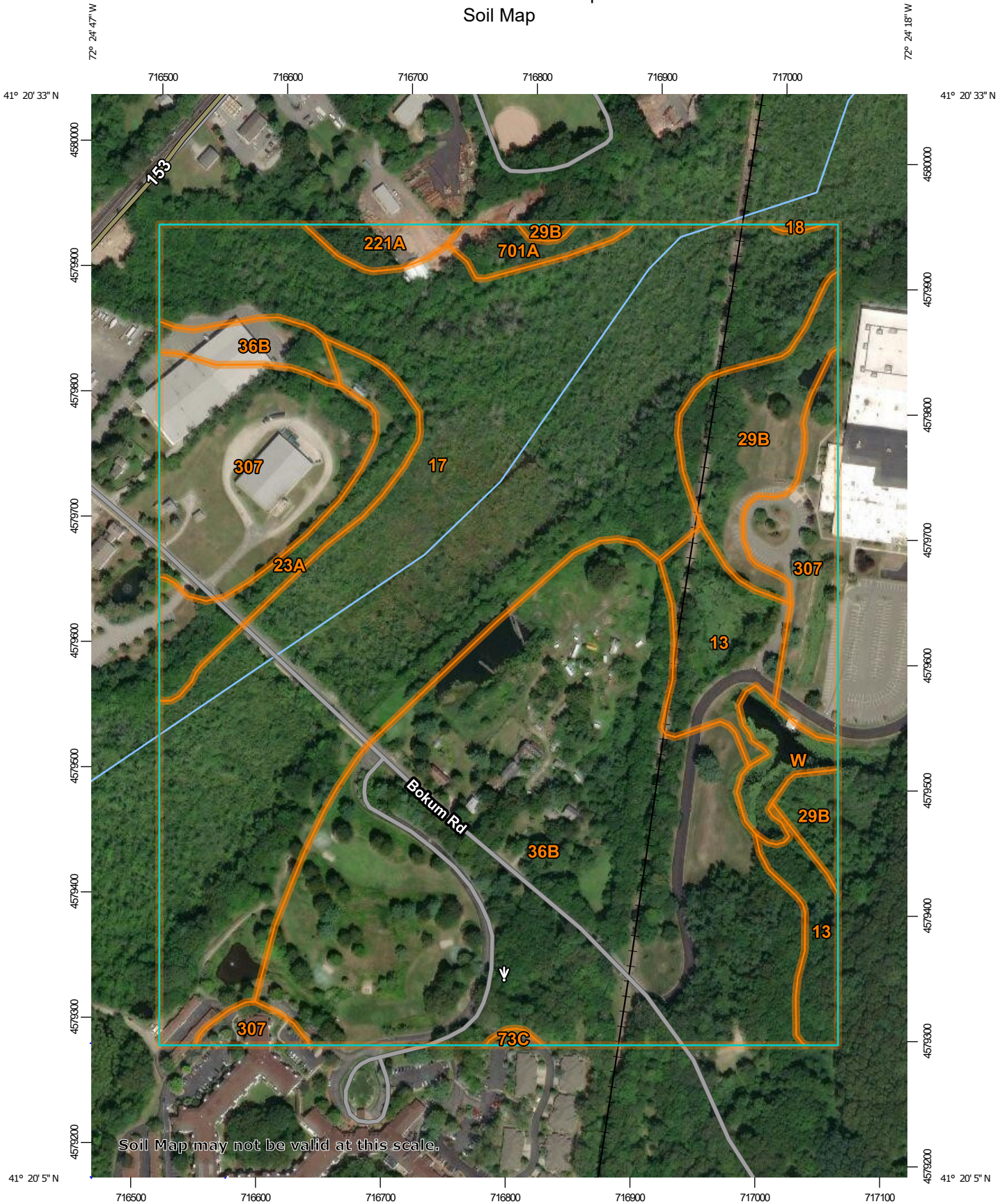
Hydrograph





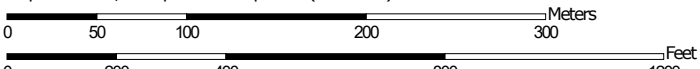


Custom Soil Resource Report  
Soil Map



Soil Map may not be valid at this scale.

Map Scale: 1:4,210 if printed on A portrait (8.5" x 11") sheet.




Map projection: Web Mercator Corner coordinates: WGS84 Edge tics: UTM Zone 18N WGS84





### MAP LEGEND

**Area of Interest (AOI)**

 Area of Interest (AOI)


**Soils**


 Soil Map Unit Polygons


 Soil Map Unit Lines


 Soil Map Unit Points

**Special Point Features**

 Blowout

 Borrow Pit


 Clay Spot


 Closed Depression

 Gravel Pit

 Gravelly Spot


 Landfill

 Lava Flow

 Marsh or swamp

 Mine or Quarry

 Miscellaneous Water


 Perennial Water

 Rock Outcrop


 Saline Spot

 Sandy Spot

 Severely Eroded Spot


 Sinkhole


 Slide or Slip


 Sodic Spot


 Spoil Area

 Stony Spot


 Very Stony Spot

 Wet Spot

 Other

 Special Line Features

**Water Features**

 Streams and Canals


**Transportation**

 Rails


 Interstate Highways

 US Routes

 Major Roads

 Local Roads

**Background**

 Aerial Photography

### MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:12,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service  
 Web Soil Survey URL:  
 Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: State of Connecticut  
 Survey Area Data: Version 20, Jun 9, 2020

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Dec 31, 2009—Sep 6, 2017

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

## Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
13	Walpole sandy loam, 0 to 3 percent slopes	4.2	4.8%
17	Timakwa and Natchaug soils, 0 to 2 percent slopes	34.1	38.6%
18	Catden and Freetown soils, 0 to 2 percent slopes	0.0	0.0%
23A	Sudbury sandy loam, 0 to 5 percent slopes	2.7	3.1%
29B	Agawam fine sandy loam, 3 to 8 percent slopes	4.4	4.9%
36B	Windsor loamy sand, 3 to 8 percent slopes	30.2	34.1%
73C	Charlton-Chatfield complex, 0 to 15 percent slopes, very rocky	0.1	0.1%
221A	Ninigret-Urban land complex, 0 to 5 percent slopes	0.8	0.9%
307	Urban land	9.9	11.2%
701A	Ninigret fine sandy loam, 0 to 3 percent slopes	0.9	1.0%
W	Water	1.2	1.3%
<b>Totals for Area of Interest</b>		<b>88.3</b>	<b>100.0%</b>

## Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a

## Custom Soil Resource Report

particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

## Custom Soil Resource Report

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

## State of Connecticut

### 13—Walpole sandy loam, 0 to 3 percent slopes

#### Map Unit Setting

*National map unit symbol:* 2svkl

*Elevation:* 0 to 1,020 feet

*Mean annual precipitation:* 36 to 71 inches

*Mean annual air temperature:* 39 to 55 degrees F

*Frost-free period:* 140 to 250 days

*Farmland classification:* Farmland of statewide importance

#### Map Unit Composition

*Walpole and similar soils:* 80 percent

*Minor components:* 20 percent

*Estimates are based on observations, descriptions, and transects of the mapunit.*

#### Description of Walpole

##### Setting

*Landform:* Outwash terraces, outwash plains, depressions, deltas, depressions

*Landform position (two-dimensional):* Toeslope

*Landform position (three-dimensional):* Tread, dip, talf

*Down-slope shape:* Concave

*Across-slope shape:* Concave

*Parent material:* Sandy glaciofluvial deposits derived from igneous, metamorphic and sedimentary rock

##### Typical profile

*Oe - 0 to 1 inches:* mucky peat

*A - 1 to 7 inches:* sandy loam

*Bg - 7 to 21 inches:* sandy loam

*BC - 21 to 25 inches:* gravelly sandy loam

*C - 25 to 65 inches:* very gravelly sand

##### Properties and qualities

*Slope:* 0 to 3 percent

*Depth to restrictive feature:* More than 80 inches

*Drainage class:* Poorly drained

*Runoff class:* Very high

*Capacity of the most limiting layer to transmit water (Ksat):* Moderately low to high  
(0.14 to 14.17 in/hr)

*Depth to water table:* About 0 to 4 inches

*Frequency of flooding:* None

*Frequency of ponding:* None

*Maximum salinity:* Nonsaline (0.0 to 1.9 mmhos/cm)

*Available water capacity:* Moderate (about 6.4 inches)

##### Interpretive groups

*Land capability classification (irrigated):* None specified

*Land capability classification (nonirrigated):* 4w

*Hydrologic Soil Group:* B/D

*Ecological site:* F144AY028MA - Wet Outwash

*Hydric soil rating:* Yes

## Minor Components

### Sudbury

*Percent of map unit:* 10 percent  
*Landform:* Deltas, outwash plains, terraces  
*Landform position (two-dimensional):* Footslope  
*Landform position (three-dimensional):* Tread, dip  
*Down-slope shape:* Concave  
*Across-slope shape:* Linear  
*Hydric soil rating:* No

### Scarboro

*Percent of map unit:* 10 percent  
*Landform:* Outwash terraces, deltas, outwash plains  
*Landform position (two-dimensional):* Toeslope  
*Landform position (three-dimensional):* Tread, dip  
*Down-slope shape:* Concave  
*Across-slope shape:* Concave  
*Hydric soil rating:* Yes

## 17—Timakwa and Natchaug soils, 0 to 2 percent slopes

### Map Unit Setting

*National map unit symbol:* 2t2qx  
*Elevation:* 0 to 1,420 feet  
*Mean annual precipitation:* 36 to 71 inches  
*Mean annual air temperature:* 39 to 55 degrees F  
*Frost-free period:* 140 to 240 days  
*Farmland classification:* Not prime farmland

### Map Unit Composition

*Timakwa and similar soils:* 45 percent  
*Natchaug and similar soils:* 40 percent  
*Minor components:* 15 percent  
*Estimates are based on observations, descriptions, and transects of the mapunit.*

### Description of Timakwa

#### Setting

*Landform:* Depressions  
*Landform position (three-dimensional):* Tread  
*Down-slope shape:* Concave  
*Across-slope shape:* Concave  
*Parent material:* Herbaceous and woody organic material over sandy and gravelly glaciofluvial deposits

#### Typical profile

*Oa1 - 0 to 12 inches:* muck  
*Oa2 - 12 to 37 inches:* muck  
*2Cg1 - 37 to 47 inches:* very gravelly loamy coarse sand

## Custom Soil Resource Report

2Cg2 - 47 to 60 inches: gravelly loamy very fine sand

### Properties and qualities

*Slope:* 0 to 2 percent

*Depth to restrictive feature:* More than 80 inches

*Drainage class:* Very poorly drained

*Runoff class:* Negligible

*Capacity of the most limiting layer to transmit water (Ksat):* Moderately low to high  
(0.14 to 14.17 in/hr)

*Depth to water table:* About 0 to 12 inches

*Frequency of flooding:* NoneRare

*Frequency of ponding:* Frequent

*Maximum salinity:* Nonsaline (0.0 to 1.9 mmhos/cm)

*Available water capacity:* Very high (about 14.9 inches)

### Interpretive groups

*Land capability classification (irrigated):* None specified

*Land capability classification (nonirrigated):* 5w

*Hydrologic Soil Group:* B/D

*Ecological site:* F144AY042NY - Semi-Rich Organic Wetlands

*Hydric soil rating:* Yes

## Description of Natchaug

### Setting

*Landform:* Depressions, depressions, depressions

*Landform position (two-dimensional):* Toeslope

*Landform position (three-dimensional):* Base slope, tread

*Down-slope shape:* Concave

*Across-slope shape:* Concave

*Parent material:* Highly decomposed organic material over loamy glaciofluvial deposits and/or loamy glaciolacustrine deposits and/or loamy till

### Typical profile

*Oa1 - 0 to 12 inches:* muck

*Oa2 - 12 to 31 inches:* muck

*2Cg1 - 31 to 39 inches:* silt loam

*2Cg2 - 39 to 79 inches:* fine sandy loam

### Properties and qualities

*Slope:* 0 to 2 percent

*Depth to restrictive feature:* More than 80 inches

*Drainage class:* Very poorly drained

*Runoff class:* Negligible

*Capacity of the most limiting layer to transmit water (Ksat):* Moderately low to high  
(0.01 to 14.17 in/hr)

*Depth to water table:* About 0 to 12 inches

*Frequency of flooding:* RareNone

*Frequency of ponding:* Frequent

*Calcium carbonate, maximum content:* 25 percent

*Maximum salinity:* Nonsaline (0.0 to 1.9 mmhos/cm)

*Available water capacity:* Very high (about 17.9 inches)

### Interpretive groups

*Land capability classification (irrigated):* None specified

*Land capability classification (nonirrigated):* 5w

*Hydrologic Soil Group:* B/D

## Custom Soil Resource Report

*Ecological site:* F144AY042NY - Semi-Rich Organic Wetlands  
*Hydric soil rating:* Yes

### Minor Components

#### Whitman

*Percent of map unit:* 7 percent  
*Landform:* Depressions, drainageways  
*Landform position (two-dimensional):* Toeslope  
*Landform position (three-dimensional):* Base slope  
*Down-slope shape:* Concave  
*Across-slope shape:* Concave  
*Hydric soil rating:* Yes

#### Catden

*Percent of map unit:* 3 percent  
*Landform:* Kettles, depressions, fens, depressions, depressions, swamps, bogs, marshes  
*Landform position (three-dimensional):* Base slope, tread  
*Down-slope shape:* Concave  
*Across-slope shape:* Concave  
*Hydric soil rating:* Yes

#### Maybid

*Percent of map unit:* 3 percent  
*Landform:* Depressions, terraces, drainageways  
*Landform position (three-dimensional):* Dip  
*Down-slope shape:* Concave  
*Across-slope shape:* Concave  
*Hydric soil rating:* Yes

#### Scarboro

*Percent of map unit:* 2 percent  
*Landform:* Drainageways, outwash terraces, depressions, outwash deltas  
*Landform position (two-dimensional):* Toeslope  
*Landform position (three-dimensional):* Base slope, tread, dip  
*Down-slope shape:* Concave  
*Across-slope shape:* Linear, concave  
*Hydric soil rating:* Yes

## 18—Catden and Freetown soils, 0 to 2 percent slopes

### Map Unit Setting

*National map unit symbol:* 2t2r2  
*Elevation:* 0 to 1,390 feet  
*Mean annual precipitation:* 36 to 71 inches  
*Mean annual air temperature:* 39 to 55 degrees F  
*Frost-free period:* 140 to 240 days  
*Farmland classification:* Not prime farmland



## Custom Soil Resource Report

*Landform position (three-dimensional):* Head slope, nose slope, side slope, crest, rise

*Down-slope shape:* Convex

*Across-slope shape:* Convex, linear

*Hydric soil rating:* No

### **Merrimac**

*Percent of map unit:* 3 percent

*Landform:* Kames, eskers, moraines, outwash terraces, outwash plains

*Landform position (two-dimensional):* Backslope, footslope, shoulder, summit

*Landform position (three-dimensional):* Side slope, crest, riser, tread

*Down-slope shape:* Convex

*Across-slope shape:* Convex

*Hydric soil rating:* No

### **Windsor**

*Percent of map unit:* 2 percent

*Landform:* Deltas, outwash plains, dunes, outwash terraces

*Landform position (three-dimensional):* Riser, tread

*Down-slope shape:* Linear, convex

*Across-slope shape:* Linear, convex

*Hydric soil rating:* No

## **36B—Windsor loamy sand, 3 to 8 percent slopes**

### **Map Unit Setting**

*National map unit symbol:* 2svkf

*Elevation:* 0 to 1,210 feet

*Mean annual precipitation:* 36 to 71 inches

*Mean annual air temperature:* 39 to 55 degrees F

*Frost-free period:* 140 to 240 days

*Farmland classification:* Farmland of statewide importance

### **Map Unit Composition**

*Windsor, loamy sand, and similar soils:* 85 percent

*Minor components:* 15 percent

*Estimates are based on observations, descriptions, and transects of the mapunit.*

### **Description of Windsor, Loamy Sand**

#### **Setting**

*Landform:* Outwash terraces, deltas, outwash plains, dunes

*Landform position (three-dimensional):* Tread, riser

*Down-slope shape:* Linear, convex

*Across-slope shape:* Linear, convex

*Parent material:* Loose sandy glaciofluvial deposits derived from granite and/or loose sandy glaciofluvial deposits derived from schist and/or loose sandy glaciofluvial deposits derived from gneiss

#### **Typical profile**

*O - 0 to 1 inches:* moderately decomposed plant material

## Custom Soil Resource Report

*A - 1 to 3 inches:* loamy sand  
*Bw - 3 to 25 inches:* loamy sand  
*C - 25 to 65 inches:* sand

### Properties and qualities

*Slope:* 3 to 8 percent  
*Depth to restrictive feature:* More than 80 inches  
*Drainage class:* Excessively drained  
*Runoff class:* Low  
*Capacity of the most limiting layer to transmit water (Ksat):* Moderately high to very high (1.42 to 99.90 in/hr)  
*Depth to water table:* More than 80 inches  
*Frequency of flooding:* None  
*Frequency of ponding:* None  
*Maximum salinity:* Nonsaline (0.0 to 1.9 mmhos/cm)  
*Available water capacity:* Low (about 4.5 inches)

### Interpretive groups

*Land capability classification (irrigated):* None specified  
*Land capability classification (nonirrigated):* 2s  
*Hydrologic Soil Group:* A  
*Ecological site:* F144AY022MA - Dry Outwash  
*Hydric soil rating:* No

### Minor Components

#### Hinckley, loamy sand

*Percent of map unit:* 10 percent  
*Landform:* Eskers, kames, deltas, outwash plains  
*Landform position (two-dimensional):* Summit, shoulder, backslope  
*Landform position (three-dimensional):* Nose slope, side slope, crest, head slope, rise  
*Down-slope shape:* Convex  
*Across-slope shape:* Convex, linear  
*Hydric soil rating:* No

#### Deerfield, loamy sand

*Percent of map unit:* 5 percent  
*Landform:* Outwash plains, terraces, deltas  
*Landform position (two-dimensional):* Footslope  
*Landform position (three-dimensional):* Tread, talf  
*Down-slope shape:* Linear  
*Across-slope shape:* Linear  
*Hydric soil rating:* No

## 73C—Charlton-Chatfield complex, 0 to 15 percent slopes, very rocky

### Map Unit Setting

*National map unit symbol:* 2w698  
*Elevation:* 0 to 1,550 feet  
*Mean annual precipitation:* 36 to 71 inches





**POINT PRECIPITATION FREQUENCY ESTIMATES**

Sanja Perica, Sandra Pavlovic, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Orlan Wilhite

NOAA, National Weather Service, Silver Spring, Maryland

[PF\\_tabular](#) | [PF\\_graphical](#) | [Maps & aerials](#)

**PF tabular**

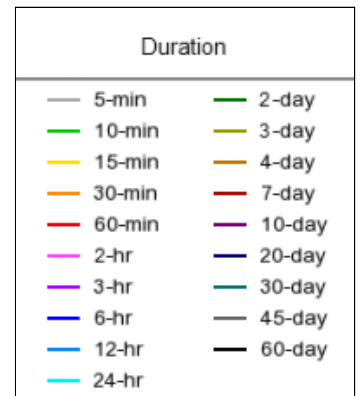
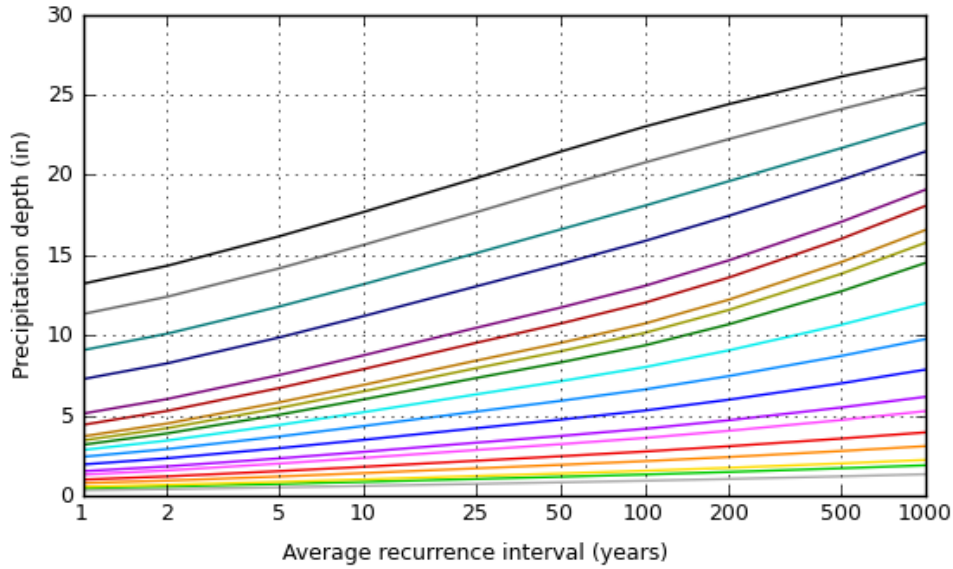
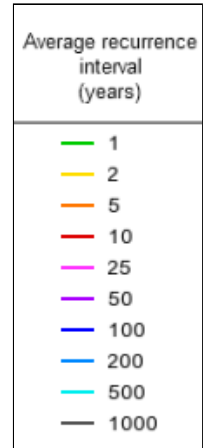
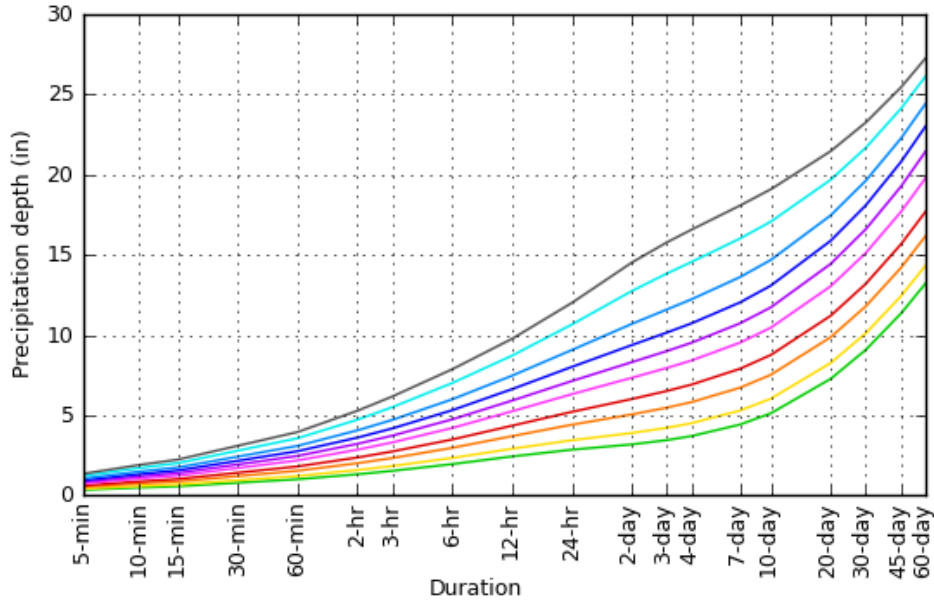
<b>PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches)<sup>1</sup></b>										
Duration	Average recurrence interval (years)									
	1	2	5	10	25	50	100	200	500	1000
<b>5-min</b>	<b>0.338</b> (0.259-0.436)	<b>0.406</b> (0.311-0.523)	<b>0.517</b> (0.394-0.667)	<b>0.610</b> (0.462-0.791)	<b>0.737</b> (0.543-0.989)	<b>0.832</b> (0.601-1.13)	<b>0.932</b> (0.657-1.31)	<b>1.05</b> (0.700-1.49)	<b>1.21</b> (0.780-1.76)	<b>1.34</b> (0.847-1.99)
<b>10-min</b>	<b>0.479</b> (0.367-0.617)	<b>0.576</b> (0.440-0.742)	<b>0.734</b> (0.560-0.948)	<b>0.864</b> (0.655-1.12)	<b>1.04</b> (0.769-1.40)	<b>1.18</b> (0.853-1.61)	<b>1.32</b> (0.931-1.86)	<b>1.48</b> (0.992-2.11)	<b>1.71</b> (1.11-2.50)	<b>1.90</b> (1.20-2.82)
<b>15-min</b>	<b>0.564</b> (0.431-0.726)	<b>0.677</b> (0.518-0.872)	<b>0.862</b> (0.656-1.11)	<b>1.02</b> (0.770-1.32)	<b>1.23</b> (0.904-1.65)	<b>1.39</b> (1.00-1.89)	<b>1.55</b> (1.10-2.18)	<b>1.74</b> (1.17-2.48)	<b>2.01</b> (1.30-2.94)	<b>2.23</b> (1.41-3.32)
<b>30-min</b>	<b>0.784</b> (0.599-1.01)	<b>0.940</b> (0.719-1.21)	<b>1.20</b> (0.912-1.55)	<b>1.41</b> (1.07-1.83)	<b>1.70</b> (1.25-2.29)	<b>1.92</b> (1.39-2.62)	<b>2.15</b> (1.52-3.03)	<b>2.41</b> (1.62-3.44)	<b>2.79</b> (1.80-4.07)	<b>3.09</b> (1.96-4.59)
<b>60-min</b>	<b>1.00</b> (0.767-1.29)	<b>1.20</b> (0.920-1.55)	<b>1.53</b> (1.17-1.98)	<b>1.80</b> (1.37-2.34)	<b>2.18</b> (1.60-2.92)	<b>2.46</b> (1.78-3.35)	<b>2.75</b> (1.94-3.87)	<b>3.09</b> (2.07-4.39)	<b>3.56</b> (2.30-5.21)	<b>3.95</b> (2.50-5.86)
<b>2-hr</b>	<b>1.31</b> (1.01-1.68)	<b>1.58</b> (1.21-2.02)	<b>2.00</b> (1.54-2.57)	<b>2.36</b> (1.80-3.04)	<b>2.85</b> (2.11-3.80)	<b>3.21</b> (2.34-4.36)	<b>3.60</b> (2.56-5.04)	<b>4.05</b> (2.72-5.73)	<b>4.72</b> (3.06-6.85)	<b>5.28</b> (3.35-7.77)
<b>3-hr</b>	<b>1.53</b> (1.18-1.94)	<b>1.83</b> (1.41-2.33)	<b>2.33</b> (1.79-2.97)	<b>2.74</b> (2.09-3.51)	<b>3.30</b> (2.46-4.39)	<b>3.72</b> (2.72-5.04)	<b>4.18</b> (2.98-5.83)	<b>4.71</b> (3.17-6.62)	<b>5.50</b> (3.58-7.95)	<b>6.17</b> (3.92-9.05)
<b>6-hr</b>	<b>1.95</b> (1.51-2.46)	<b>2.33</b> (1.81-2.95)	<b>2.96</b> (2.29-3.76)	<b>3.48</b> (2.68-4.44)	<b>4.20</b> (3.15-5.55)	<b>4.74</b> (3.48-6.37)	<b>5.31</b> (3.81-7.37)	<b>5.99</b> (4.05-8.37)	<b>7.01</b> (4.57-10.0)	<b>7.86</b> (5.02-11.4)
<b>12-hr</b>	<b>2.42</b> (1.90-3.05)	<b>2.91</b> (2.27-3.65)	<b>3.69</b> (2.88-4.65)	<b>4.34</b> (3.37-5.50)	<b>5.24</b> (3.95-6.87)	<b>5.91</b> (4.37-7.88)	<b>6.63</b> (4.77-9.11)	<b>7.47</b> (5.07-10.3)	<b>8.71</b> (5.71-12.4)	<b>9.77</b> (6.25-14.1)
<b>24-hr</b>	<b>2.85</b> (2.24-3.55)	<b>3.44</b> (2.71-4.29)	<b>4.41</b> (3.45-5.52)	<b>5.21</b> (4.06-6.55)	<b>6.31</b> (4.78-8.23)	<b>7.13</b> (5.30-9.46)	<b>8.01</b> (5.82-11.0)	<b>9.07</b> (6.19-12.5)	<b>10.7</b> (7.00-15.0)	<b>12.0</b> (7.71-17.2)
<b>2-day</b>	<b>3.18</b> (2.52-3.94)	<b>3.89</b> (3.08-4.82)	<b>5.05</b> (3.98-6.27)	<b>6.01</b> (4.71-7.50)	<b>7.33</b> (5.60-9.51)	<b>8.31</b> (6.23-11.0)	<b>9.37</b> (6.87-12.8)	<b>10.7</b> (7.32-14.6)	<b>12.7</b> (8.40-17.8)	<b>14.5</b> (9.36-20.6)
<b>3-day</b>	<b>3.44</b> (2.74-4.25)	<b>4.21</b> (3.35-5.20)	<b>5.47</b> (4.33-6.77)	<b>6.51</b> (5.13-8.09)	<b>7.94</b> (6.08-10.3)	<b>9.00</b> (6.77-11.8)	<b>10.2</b> (7.47-13.8)	<b>11.6</b> (7.95-15.7)	<b>13.8</b> (9.13-19.3)	<b>15.8</b> (10.2-22.3)
<b>4-day</b>	<b>3.70</b> (2.95-4.55)	<b>4.50</b> (3.59-5.55)	<b>5.82</b> (4.62-7.18)	<b>6.91</b> (5.46-8.57)	<b>8.41</b> (6.46-10.8)	<b>9.52</b> (7.18-12.5)	<b>10.7</b> (7.90-14.6)	<b>12.2</b> (8.40-16.6)	<b>14.6</b> (9.63-20.2)	<b>16.6</b> (10.7-23.3)
<b>7-day</b>	<b>4.42</b> (3.54-5.40)	<b>5.29</b> (4.24-6.48)	<b>6.71</b> (5.36-8.24)	<b>7.90</b> (6.27-9.73)	<b>9.52</b> (7.34-12.2)	<b>10.7</b> (8.11-13.9)	<b>12.0</b> (8.86-16.1)	<b>13.6</b> (9.39-18.3)	<b>16.0</b> (10.6-22.1)	<b>18.1</b> (11.7-25.3)
<b>10-day</b>	<b>5.12</b> (4.12-6.24)	<b>6.03</b> (4.85-7.36)	<b>7.52</b> (6.02-9.20)	<b>8.76</b> (6.97-10.7)	<b>10.5</b> (8.07-13.3)	<b>11.7</b> (8.87-15.1)	<b>13.1</b> (9.63-17.4)	<b>14.7</b> (10.2-19.6)	<b>17.1</b> (11.4-23.4)	<b>19.1</b> (12.4-26.6)
<b>20-day</b>	<b>7.27</b> (5.89-8.80)	<b>8.25</b> (6.68-10.0)	<b>9.87</b> (7.96-12.0)	<b>11.2</b> (8.98-13.7)	<b>13.0</b> (10.1-16.4)	<b>14.4</b> (10.9-18.4)	<b>15.9</b> (11.6-20.7)	<b>17.5</b> (12.2-23.1)	<b>19.7</b> (13.2-26.7)	<b>21.5</b> (14.0-29.6)
<b>30-day</b>	<b>9.07</b> (7.38-10.9)	<b>10.1</b> (8.21-12.2)	<b>11.8</b> (9.55-14.3)	<b>13.2</b> (10.6-16.0)	<b>15.1</b> (11.7-18.8)	<b>16.6</b> (12.6-20.9)	<b>18.1</b> (13.2-23.3)	<b>19.6</b> (13.7-25.9)	<b>21.7</b> (14.5-29.3)	<b>23.2</b> (15.2-31.9)
<b>45-day</b>	<b>11.3</b> (9.25-13.6)	<b>12.4</b> (10.1-14.9)	<b>14.2</b> (11.5-17.1)	<b>15.6</b> (12.6-18.9)	<b>17.7</b> (13.8-21.8)	<b>19.2</b> (14.6-24.1)	<b>20.8</b> (15.2-26.5)	<b>22.2</b> (15.6-29.2)	<b>24.1</b> (16.2-32.4)	<b>25.4</b> (16.6-34.7)
<b>60-day</b>	<b>13.2</b> (10.8-15.8)	<b>14.3</b> (11.7-17.2)	<b>16.2</b> (13.2-19.4)	<b>17.7</b> (14.3-21.3)	<b>19.8</b> (15.4-24.3)	<b>21.4</b> (16.3-26.7)	<b>23.0</b> (16.8-29.1)	<b>24.4</b> (17.2-31.9)	<b>26.1</b> (17.6-35.0)	<b>27.3</b> (17.9-37.1)

<sup>1</sup> Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS). Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.

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**PF graphical**

PDS-based depth-duration-frequency (DDF) curves  
 Latitude: 41.3393°, Longitude: -72.4089°



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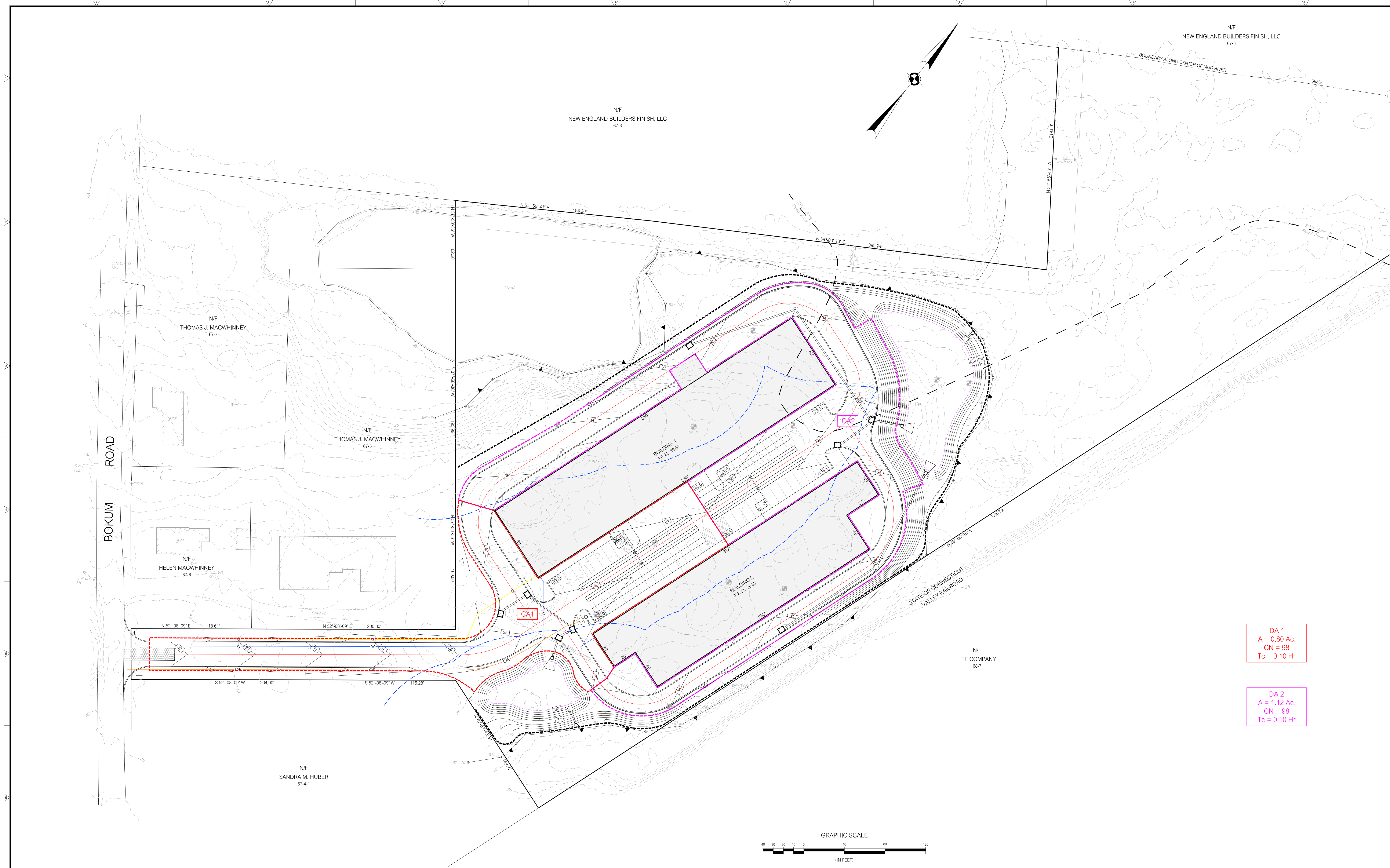
**Maps & aerials**

**Small scale terrain**

Appendix E  
Catchment Area Map

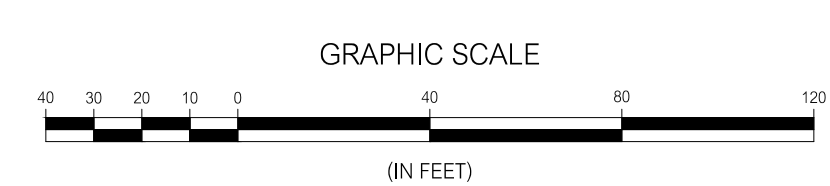
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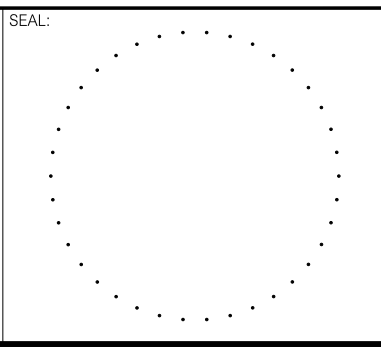
DA 1  
A = 0.80 Ac.  
CN = 98  
Tc = 0.10 Hr

DA 2  
A = 1.12 Ac.  
CN = 98  
Tc = 0.10 Hr



NO.	DATE	DESCRIPTION
REVISIONS		

LAND OF  
GEORGE C. FIELD COMPANY, INC.  
BOKUM ROAD  
ESSEX, CONNECTICUT



Prepared by:  
**Summer Hill**  
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PROJECT: BOKUM ROAD BUSINESS PARK BOKUM ROAD ESSEX, CONNECTICUT		SHEET NO.: CA 1
DATE: 7-1-21	DESIGNED: MJU	PROJECT NO.: 20-50
SCALE: 1"=40'	CHECKED: LJM	
FIELD BOOK:		



